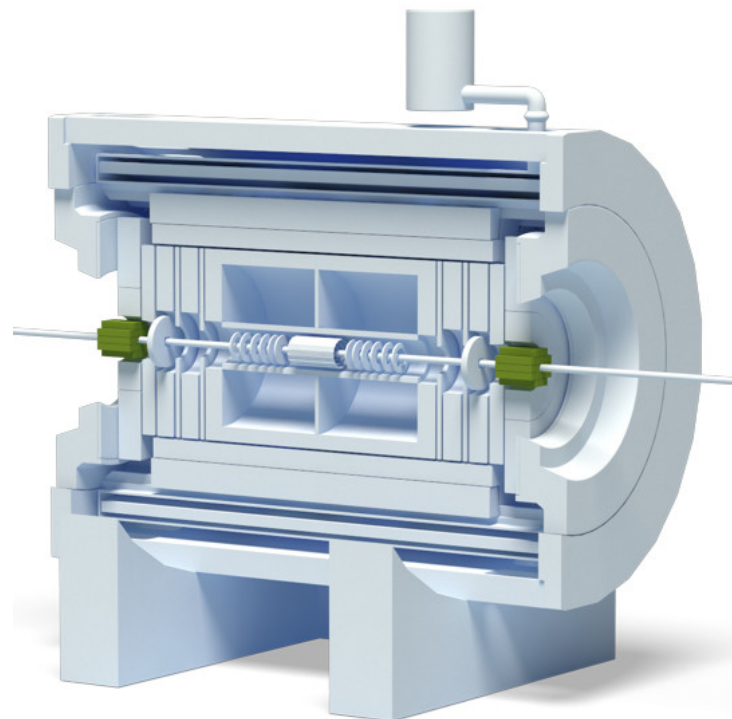




# Technical Design Report for the MPD Experiment

Nuclotron Based Ion Collider Facility

## Forward Hadron Calorimeter (FHCaI)



June 2018



# TECHNICAL DESIGN REPORT FOR THE MPD EXPERIMENT

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## Forward Hadron Calorimeter (FHCAL)

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## 12 **1 Preface**

13 This technical design report presents the layout and performance of the Forward Hadron Calorimeter  
14 (FHCAL) for the MPD experiment at the NICA accelerator facility. The main purpose of the FHCAL is to  
15 provide an experimental measurement of a heavy-ion collision centrality and orientation of its reaction  
16 plane. Precise event-by-event estimate of the collision geometry is crucial for many physics phenomena  
17 studies to be performed by the MPD Collaboration.

18 The FHCAL is a compensating lead-scintillator calorimeter designed to measure the energy distribution  
19 of the projectile nuclei fragments (spectators) and forward going particles produced close to the beam  
20 rapidity. The main design requirements of the FHCAL are (a) the larger forward rapidity coverage with  
21 sufficient energy resolution to allow for precise collision centrality determination and consequently of  
22 the number of participating nucleons and (b) sufficient granularity in the plane transverse to the beam  
23 direction for the reaction plane reconstruction. The proposed modular design of the FHCAL covers large  
24 transverse area around the beam spot position such that most of the projectile spectator fragments deposit  
25 their energy in the FHCAL.

26 Each module of the FHCAL has a lead-scintillator sandwich structure with longitudinal segmentation  
27 which can be used to separate electromagnetic and hadronic showers in the calorimeter. A lead-scintillator  
28 prototype of the FHCAL module with scintillator light readout by silicon photomultipliers (micropixel  
29 avalanche photodiodes) was tested with the proton and pion beams.

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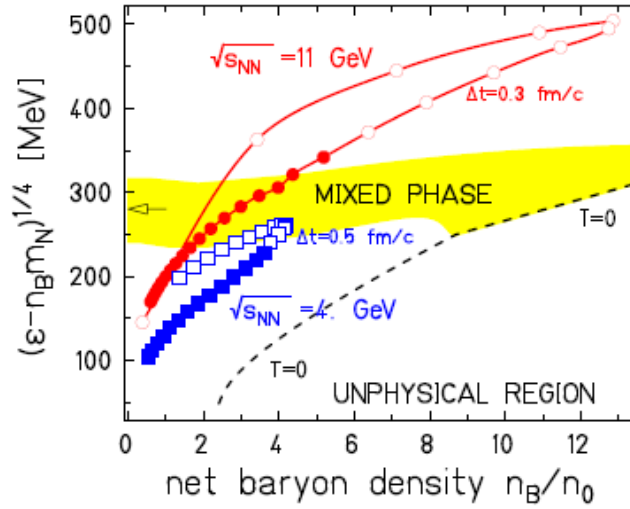
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## 82 2 Introduction

### 83 2.1 Physics motivation

84 The goal of the MPD experiment at NICA is to explore the QCD phase diagram in the region of highly  
 85 compressed and hot baryonic matter [1] in the region of the collider energy  $\sqrt{s_{NN}} = 4 - 11 \text{ GeV}$ . The ori-  
 86 gin of confinement, vacuum properties, and the (chiral) symmetries of the QCD, which still lack a quan-  
 87 titative theoretical understanding, are among the main topics of the MPD experiment studies. Figure 1  
 88 shows the dynamical trajectories for central ( $b = 2 \text{ fm}$ )  $Au + Au$  collisions at two collision energies. The  
 89 highly non-equilibrium part of trajectories are calculated within the kinetic Quark Gluon String Model  
 90 (open symbols) and the subsequent evolution is evaluated within the 3D relativistic hydrodynamics (solid  
 91 symbols). The specifics of this region is that the nuclear matter is created at the highest net baryon den-  
 92 sity. A mixed phase may be reached in this region of the phase diagram as well as a hypothetical critical  
 93 end point [2].

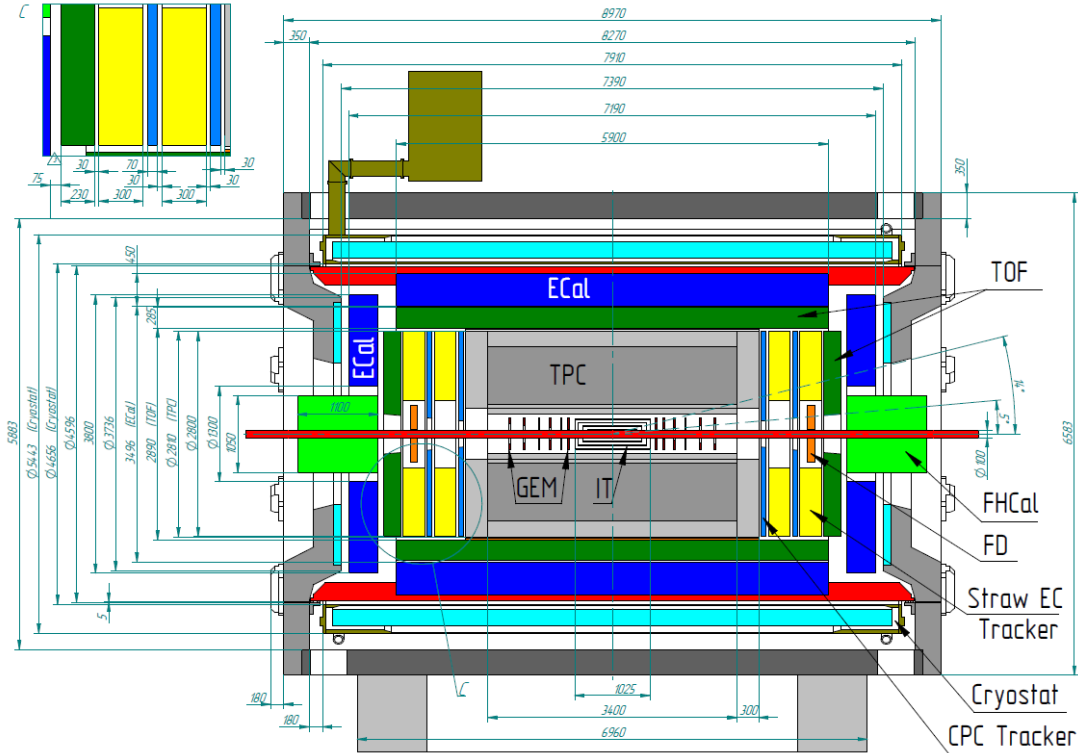


**Fig. 1:** The phase diagram in terms of the reduced energy density and net baryon density. The highlighted region is a quark-hadron mixed phase estimates according to the phenomenological two-phase equation of state [3]. The dashed curve at  $T = 0$  separates the unphysical region.

94 The basic strategy of the MPD experiment is to measure a large variety of observables for heavy-ion  
 95 collisions as a function of the collision energy, centrality, and the system size. Reference data for  $pp$   
 96 and  $pA$  collisions will be also taken at the same experimental conditions. Among the main experimental  
 97 observables [4] are the total particle yields and their ratios, event-by-event fluctuations and correlations,  
 98 collective flow of identified hadrons (in particular of anti-baryons), strangeness production, femtoscopy,  
 99 and electromagnetic probes.

### 100 2.2 MPD experiment

101 The MPD experiment has a close to  $4\pi$  acceptance and is designed to detect charged hadrons, electrons  
 102 and photons produced in heavy-ion collisions in the energy range and high luminosities of the NICA  
 103 collider. The side view of the MPD experiment is shown in Fig. 2. It includes the superconducting  
 104 solenoid, Time-Projection Chamber (TPC), Time-Of-Flight (TOF) detector, Electromagnetic Calorimeter  
 105 (ECal), Forward Hadron Calorimeter (FHCAL) and Fast Forward Detector (FFD). The main detector  
 106 components for particle tracking and identification are the TPC and TOF. At the design luminosity, the  
 107 expected event rate in the MPD is about 6 kHz. The total charged particle multiplicity is around 1000 for  
 108 the most central  $Au + Au$  collisions at the top NICA energy of  $\sqrt{s_{NN}} = 11 \text{ GeV}$  [5]. The detector design



**Fig. 2:** Side view of the MPD experiment with indicated subsystem dimensions.

109 has a very low material budget to allow for reconstruction of the typical particle transverse momentum  
 110 below 500 MeV/c expected at NICA energies.

### 111 2.3 The concept of the Forward Hadron Calorimeter (FHCAL)

112 Experimental estimate of global event characteristics in nucleus-nucleus collisions such as the centrality  
 113 of the collision which is related to the number of participating nucleons and the reaction plane orientation  
 114 are challenging tasks for any high-energy heavy-ion experiments including the MPD experiment  
 115 at NICA. In heavy-ion interactions the event-by-event determination of the collision centrality is used  
 116 to study observables like the collective flow, particle multiplicities and fluctuations which vary strongly  
 117 with centrality. The collision centrality can be determined either by the multiplicity of produced particles  
 118 in the participant zone or by measuring the energy carried by the non-interacting nucleons (projectile  
 119 spectators) and detected by forward hadron calorimeter. The measurement of the number of projectile  
 120 spectators allows to estimate the number of the participants and hence the impact parameter  $b$ , which are  
 121 strongly correlated.

122 The collective flow of particles produced in a heavy-ion collision is an important observable which  
 123 provides information about the dynamics of the reaction and the properties of the matter in the fireball  
 124 [6–8]. The flow is defined with respect to the reaction plane which is spanned by the beam direction  
 125 and the impact parameter of the collision. The orientation of the impact parameter is reflected by the  
 126 spectators, i.e. the nucleons and fragments which do not participate in the collision, which are deflected  
 127 in the direction of the impact parameter. Therefore, the most direct method to determine the reaction  
 128 plane is to measure the position and energy of the spectators at a certain distance downstream the target.

129 The FHCAL is designed for determination of the collision centrality and the orientation of the reaction  
 130 plane for collective flow studies. An event-by-event determination of these quantities is of crucial im-  
 131 portance for the analysis of many physics observables. The detector will measure the energy of non-



132 interacting nucleons and fragments (spectators) in nucleus-nucleus collisions. The FHCAL consists of  
 133 two hadron calorimeters with 45 each suited symmetrically from the interaction point. It is a fully com-  
 134 pensating modular lead-scintillator calorimeter with high and uniform energy resolution. Each individual  
 135 module consists from 42 lead/scintillator layers with a surface of  $15 \times 15 \text{ cm}^2$ . The scintillation light is  
 136 read out via wavelength shifting (WLS) fibers by silicon photomultipliers (SiPM) (multipixel avalanche  
 137 photodiodes (MAPD)).

## 138 2.4 Requirements to FHCAL

139 The FHCAL must have both appropriate energy resolution and modular structure with high enough trans-  
 140 verse granularity to measure the event-by-event centroid of the spectator distribution. The main require-  
 141 ments to the FHCAL performance are:

- 142 – Spectators detection in the energy range 1 – 6 GeV.
- 143 – Operation at the trigger rates up to 6 kHz.
- 144 – Reaction plane determination using particles produced at forward rapidity with accuracy close to  
 145 that of ideal tracking detector at flow signals and multiplicities in heavy-ion collisions expected at  
 146 NICA energies.
- 147 – Collision centrality determination using particles produced at forward rapidity with impact param-  
 148 eter resolution between 5-10% for (mid-)central collisions.

149 As will be shown later in this document, these requirements are met with the following FHCAL properties:

- 150 – Large transverse area (of the order of  $1 \times 1 \text{ m}^2$ ) to register the collision spectators at beam energies  
 151 of a few  $A \text{ GeV}$ .
- 152 – Energy resolution:  $\frac{\sigma_E}{E} < \frac{60\%}{\sqrt{E(\text{GeV})}}$ .
- 153 – Good uniformity of the detector response
- 154 – High transverse segmentation
- 155 – Operation in a solenoid magnet field

156 Operation in the solenoid magnet field implies that FHCAL is constructed out of nonmagnetic materials  
 157 and has an appropriate readout parts. As can be seen from Fig. 2, a very limited space inside the magnet  
 158 constrains the total length of FHCAL to be about 1 m.

## 159 2.5 Detector concept

160 In order to fulfill the FHCAL design requirements the compensating hadron calorimeter is proposed. The  
 161 concept of compensating calorimeter was intensively developed last years with the understanding of the  
 162 physical processes inside the hadron shower. The hadron shower in some absorber consists in reality of  
 163 two, electromagnetic ( $e$ ) and pure hadronic ( $h$ ) shower components. The hadronic component originates  
 164 from neutral pions produced in nuclear interactions and is the dominant source of the shower profile  
 165 fluctuations. The energy sharing between the  $e$  and  $h$  components can be very different from event to  
 166 event and depends mainly on the nature of the first interaction, which will produce or not a  $\pi^0$  particle.  
 167 The equalization of the calorimeter response to the  $e$  and  $h$  components ( $e/h = 1$ ), called the compen-  
 168 sation condition, eliminates one of the dominant source of the energy fluctuation and hence improves  
 169 the energy resolution of the calorimeter. The other advantages of the compensating calorimeters are

170 linearity and Gaussian shape signal of the detector response. This concept was first applied in uranium  
171 calorimeters [5] and later adopted to the more general cases.

172 Nowadays this approach is successfully applied to the calorimeters with the iron and/or lead absorbers [9].  
173 It was shown that the compensating condition ( $e/h = 1$ ) depends on the relative absorber/active thickness  
174 ratio. Compensating condition  $e/h = 1$  is fulfilled for Fe:Scintillator sampling ratio equal 20. The  
175 iron calorimeter cannot be used in magnet field of MPD experiment. For lead absorber sampling ratio  
176 Pb:Scintillator should be equal 4. The last case of lead/scintillator calorimeter is rather attractive due to  
177 the smaller compensating ratio and consequently smaller sampling fluctuation of the shower.

178 At present, there are a few performance measurements for the calorimeters with similar structure. One  
179 lead-scintillator compensating calorimeter with the resolution of about  $58\%/\sqrt{E}$  was used in WA97  
180 experiment at CERN [10]. This calorimeter has classical light readout with the wave-shifter plates and  
181 PMT's. Such readout suffers the Cherenkov light in the WLS-plates and nuclear counter effect in PMT's  
182 placed behind the active part of the calorimeter.

183 Another similar calorimeter prototype [11] with the finer sampling developed for JLC project has reso-  
184 lution of about  $50\%/\sqrt{E}$  and avoids such drawbacks. It uses fiber-tile readout that ensures the efficient  
185 light collection in the scintillator layers together with the perfect transverse uniformity of the energy reso-  
186 lution. At the same time, use of large amount PMT's for readout of each scintillator layer leads to the  
187 complexity and high cost of such calorimeter. Also PMT operation is very restricted in magnetic field.

188 The review of the current experimental situation reveals that a full compensating modular lead-scintillator  
189 calorimeter with sampling ratio 4 : 1 meets the above requirements and was selected for the FHCAL  
190 calorimeter. The proposed calorimeter design of the FHCAL for the MPD experiment combines the ad-  
191 vantages of the fiber-tile readout with the simplicity of the photodetectors. Each (left/right) part of FHCAL  
192 consists of 45 individual modules with the transverse size  $15 \times 15 \text{ cm}^2$  each. Each module includes 42  
193 lead/scintillator sandwiches with the total interaction length of about  $4\lambda_i$ . Every 6 consecutive layers  
194 of scintillators are readout by a single photodetector via the WLS-fibers. As a result, 7 sections with  
195 the individual light readout provide the longitudinal segmentation of FHCAL modules. The light from  
196 the WLS-fibers is readout by silicon photomultipliers (SiPM's) or micropixel avalanche photodiodes  
197 (MAPD's) instead of commonly used PMT's. In spite of relatively recent appearance this new type  
198 of photodiodes starts to be intensively used at modern setups due to their remarkable properties. Good  
199 photon detection efficiency and the gain comparable with normal PMT's, the compactness, insensitivity  
200 to magnetic field, low cost and simplicity of the operation make these devices very attractive for the  
201 different applications including the calorimetry. As shown below, the proposed FHCAL design fulfills the  
202 requirements for the MPD experiment at NICA.

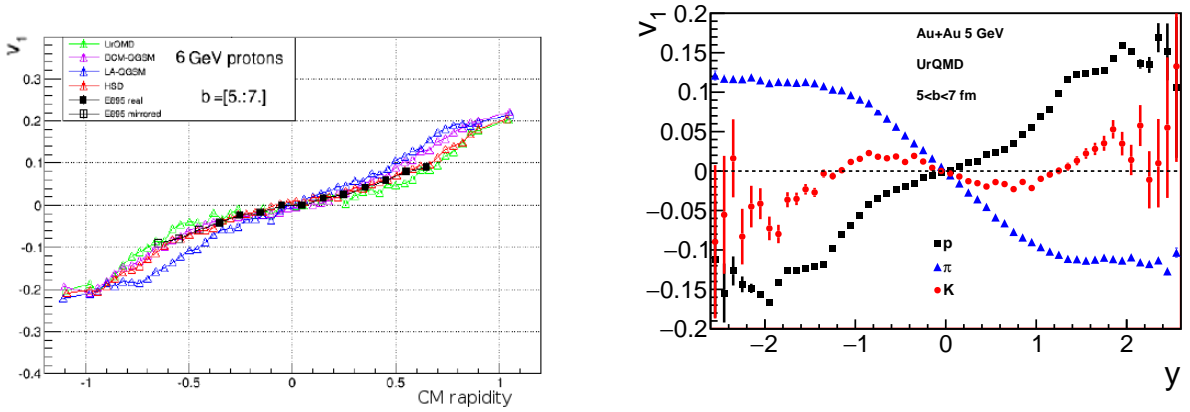
203 Recently, fully compensating modular lead-scintillator calorimeter with sampling ratio 4 : 1 with fiber-  
204 tile readout light collection and readout by micropixel avalanche photodiodes have been constructed for  
205 the NA61/SHINE experiment at CERN SPS [12–14].

### 206 3 FHCAL performance for centrality and event plane determination

#### 207 3.1 Heavy-ion event generators at NICA energies

208 The FHCAL performance for centrality and reaction plane determination is evaluated for  $Au + Au$  collisions at the center-of-mass energies  $\sqrt{s_{NN}} = 4 - 11$  GeV. The heavy-ion collisions were simulated with  
 209 LA-QGSM [15–19] and UrQMD [20, 21] event generators. The LA-QGSM code is based on a Multi  
 210 Stage Dynamical Model and includes generation of collision fragments which is a needed ingredient for  
 211 the FHCAL performance study. The fragment generation by the LA-QGSM code is in good agreement  
 212 with the experimental data [15–19].  
 213

214 Figure 3(left) shows the directed flow  $v_1$  of protons vs rapidity  $y$  calculated with different heavy-ion collision generators in comparison with the experimental data at NICA energies [22, 23]. The signals



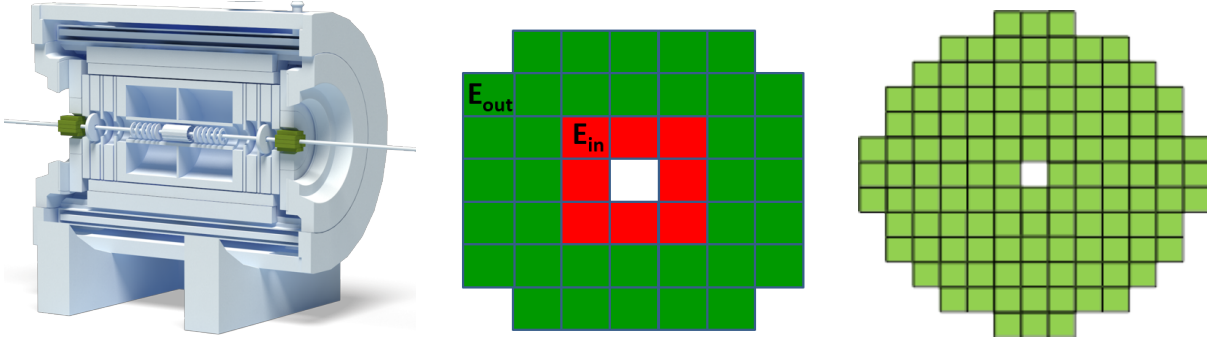
**Fig. 3:** (left) Directed flow  $v_1$  of protons vs rapidity  $y$  calculated with the UrQMD [20, 21], DCM- and LA-QGSM [15–19], HSD [24] event generators in comparison with the E895 data [25] for  $Au + Au$  collision at the beam energy 6 GeV (right). Figure adopted from [22, 23]. (right) Direct flow of spectator nucleons (protons), kaons and pions as a function of the rapidity simulated with the UrQMD model for  $Au - Au$  collisions at  $\sqrt{s_{NN}} = 5$  GeV and impact parameter range  $b = 5 - 9$  fm.

215 for  $v_1$  of protons calculated with the LA-QGSM and UrQMD models are similar to the experimental  
 216 data for  $Au$ -beam energy 6 GeV. The availability of fragments in the spectator region and the qualitative  
 217 agreement with the experimental data for directed flow makes the LA-QGSM code suitable for the FHCAL  
 218 performance study. The comparison to the simulation with the UrQMD generator which does not include  
 219 fragment generation can be used to estimate the effects of the forward fragment production on the FHCAL  
 220 performance.  
 221

222 Figure 3(right) shows the calculated with UrQMD directed flow  $v_1$  for identified hadrons (proton, kaon  
 223 and pion) in a wide rapidity range.  $v_1$  of proton and pion has opposite magnitude and increased toward  
 224 forward rapidity which will play a role in FHCAL performance for flow measurement.

#### 225 3.2 Simulation setup

226 The MPD detector geometry and its response to particles simulated with heavy-ion event generators are  
 227 implemented within a GEANT [26] Monte-Carlo simulation framework. The simulated MPD geometry  
 228 as illustrated in Fig. 4(left) includes all detectors subsystems, among those are two parts of FHCAL on left  
 229 and right sides from the center of the MPD at the distance  $3195 \times 2 = 6390$  mm. Both parts of FHCAL  
 230 consists of 44 individual modules as shown in Fig. 4(middle) with the transverse module size being  
 231  $15 \times 15$  cm<sup>2</sup>. Instead of the central module calorimeter has a hole for a beam pipe with the size  $15 \times 15$   
 232 cm<sup>2</sup>. Each module includes 42 lead/scintillator sandwiches with the total interaction length of about



**Fig. 4:** (left) The scheme of MPD (light blue) and the position of the FHCAL detector (green) inside the experiment. (middle) Transverse layout of the FHCAL with 44 individual modules and the beam hole in the center of the detector. The inner (outer) group of modules which are later used in the performance studies are indicated with the red (green) color. (right) High granularity configuration of the FHCAL (highFHCAL) transverse layout which is used for comparison studies.

233  $4\lambda_i$ . Every 6 consecutive layers of scintillators have individual readout, which provides the longitudinal  
 234 segmentation of FHCAL modules. To evaluate the effect of the MPD solenoidal magnet, the simulated  
 235 axial magnetic field of 0.5 T is uniformly distributed between the FHCAL parts.

### 236 3.2.1 High granularity FHCAL (highFHCAL)

237 The FHCAL module transverse sizes of  $15 \times 15 \text{ cm}^2$  were chosen to match the size of the hadron showers.  
 238 The production of such modules is much simpler and cheaper than that of smaller sizes. The dimensions  
 239 of the calorimeter are slightly smaller than the available space in the forward directions. This might  
 240 reduce the performance comparing to the "ideal" calorimeter with the high granularity and higher ac-  
 241 ceptance (highFHCAL). To study these effects a simulation for highFHCAL was performed with a same  
 242 simulation setup as it was for FHCAL. Its structure is presented in Fig. 4(right). It consists of 240 small  
 243 modules (120 on each side) with the transverse sizes  $10 \times 10 \text{ cm}^2$ . The calorimeter has a beam hole of  
 244  $10 \times 10 \text{ cm}^2$ .

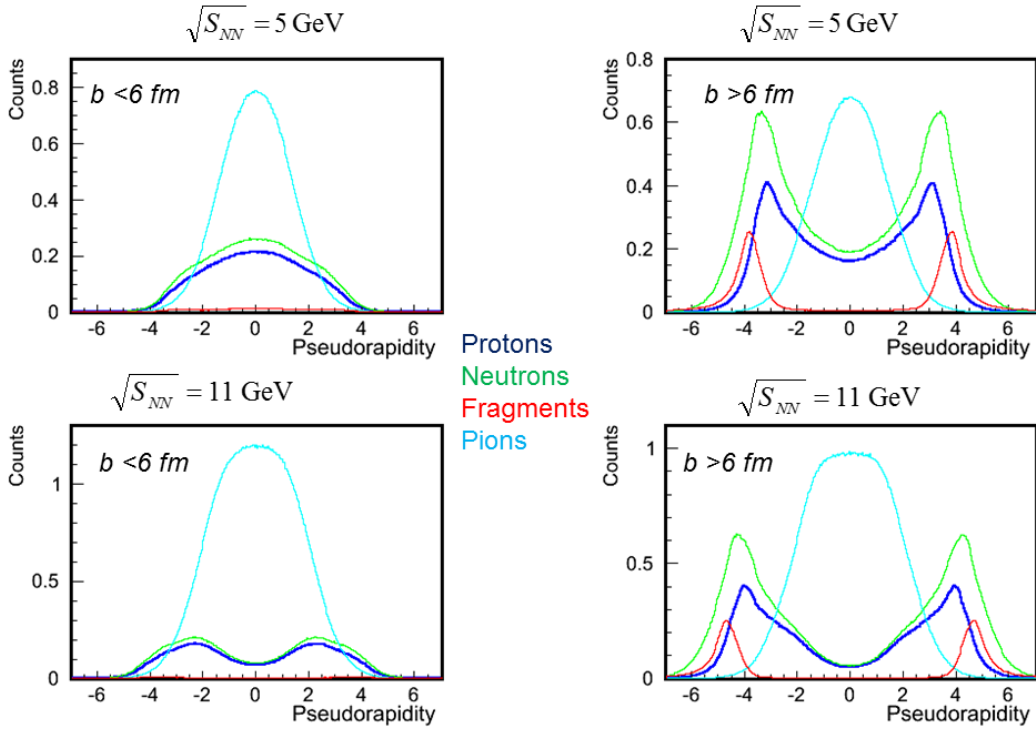
### 245 3.2.2 Forward Wall (FW) of scintillator cells

246 The simplest variant of forward detector (wall of the scintillator cells) was considered also to study the  
 247 effect of the charged particles. The energy of the particles was not measured in this case. Only the hit  
 248 points and the ionizing losses of the charged particles in the scintillator were available. Two Forward  
 249 Wall (FW) detectors were placed at the same distance from the interaction point as the FHCAL. The FW  
 250 consists of the scintillator cells with the size  $5 \times 5 \times 1 \text{ cm}^3$ . Inner and outer diameters of the FW equal  
 251 to 10 and 140 cm, respectively.

## 252 3.3 Particle abundances in the FHCAL acceptance

253 Figure 5 shows Pseudorapidity ( $\eta$ ) distributions of particles simulated with the LA-QGSM model for  
 254 collisions at  $\sqrt{s_{NN}} = 5 \text{ GeV}$  and  $\sqrt{s_{NN}} = 11 \text{ GeV}$ . Distributions for all particles as well as separately for  
 255 protons and neutrons, fragments, and pions are shown. Pseudorapidity range  $2 < |\eta| < 5$  corresponds to  
 256 FHCAL acceptance. FHCAL is mainly sensitive to spectator protons and fragments. Pion contamination is  
 257 increasing with collision energy.

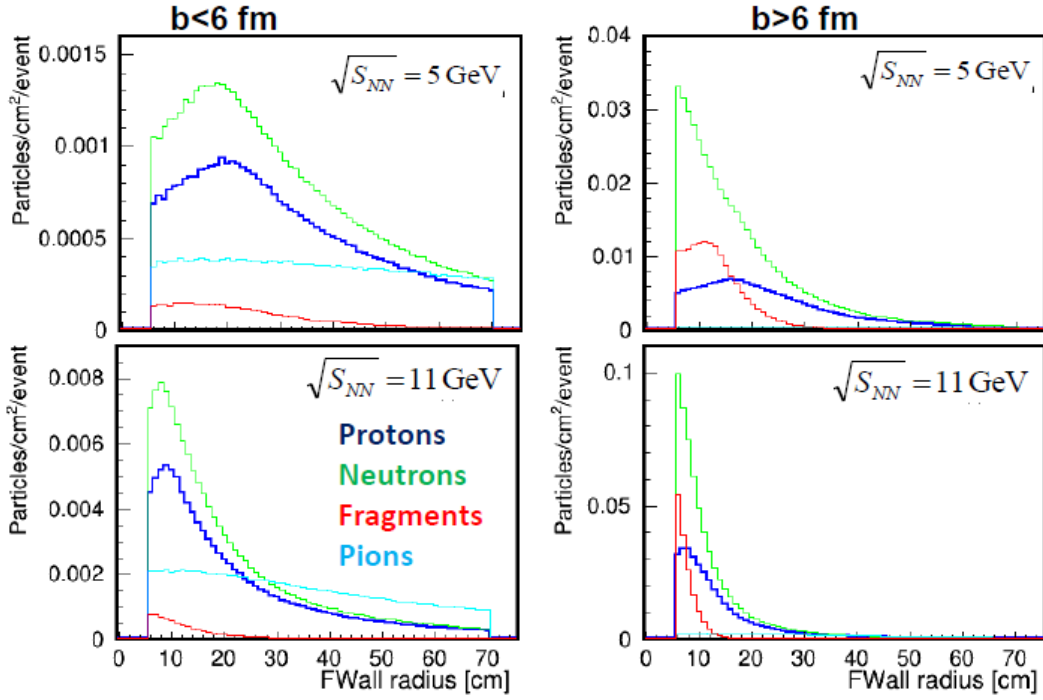
258 Figure 6 shows distribution for same types of particles as in Fig. 5 vs radial distance from the center of the  
 259 FW ( $R_{FW}$ ) at the FW  $z$  position along the beam line direction. Besides the spectators (protons, neutron  
 260 and fragments) a significant amount of the produced pions hit the detector. The fraction of the fragments  
 261 (with atomic number  $A > 2$ ) is rather small even in the peripheral collisions. The  $A$ -distributions of



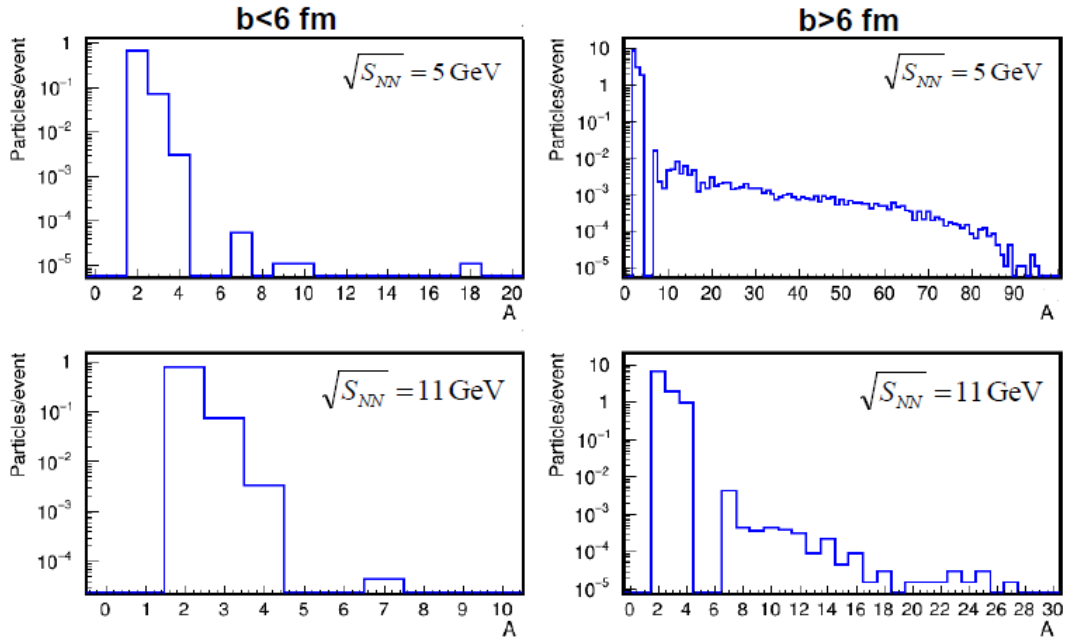
**Fig. 5:** Pseudorapidity distribution of different particles for  $Au - Au$  collisions for beam energies  $\sqrt{s_{NN}} = 5$  GeV (up) and  $\sqrt{s_{NN}} = 11$  GeV (down) in two event classes  $b < 6$  fm (left) and  $b > 6$  fm (right). Pseudorapidity range  $2 < |\eta| < 5$  corresponds to FHCAL acceptance.

262 fragments are shown in Fig. 7 and for two centrality regions  $b < 6$  fm and  $b > 6$  fm. The main fragments  
 263 are deuteron, tritium and helium. The contamination of heavy fragments is negligible, because they  
 264 escape into the FHCAL beam hole.

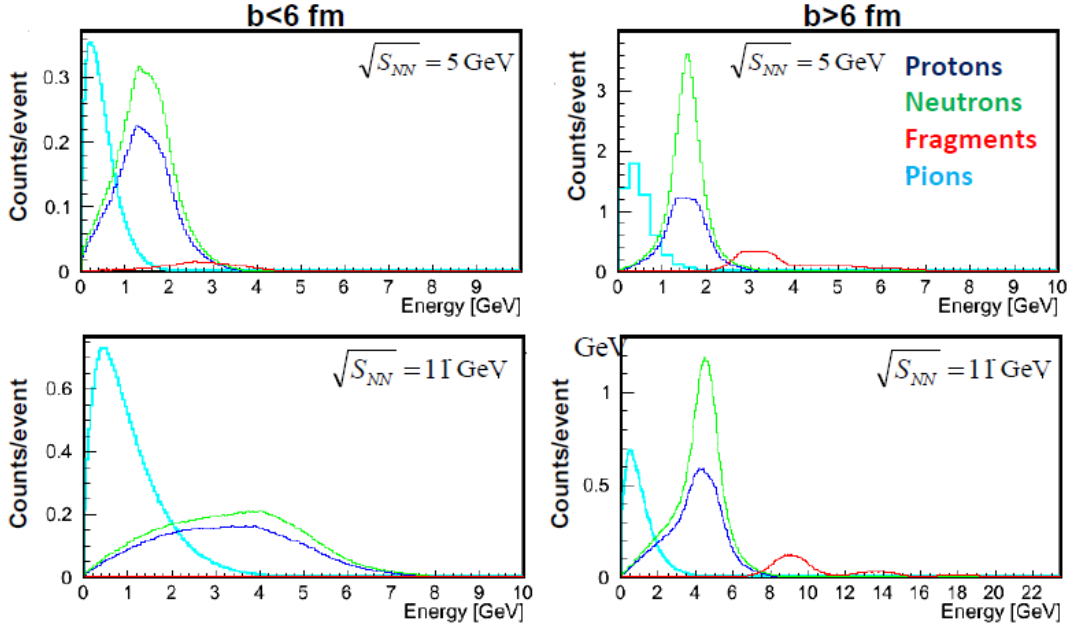
265 Energy (multiplicity) distributions for different particles are presented in Fig. 8(9). The energy of pions  
 266 are significantly smaller comparing to that of protons and neutrons. It confirms that the contributions of  
 267 the pions in the energy depositions in FHCAL are rather small. The situation is worse for the case of the  
 268 FW, where each hit from pions or protons has the same weight. The multiplicity of pions and protons are  
 269 comparable. At highest beam energy for the central events the pion multiplicity exceeds that of protons.



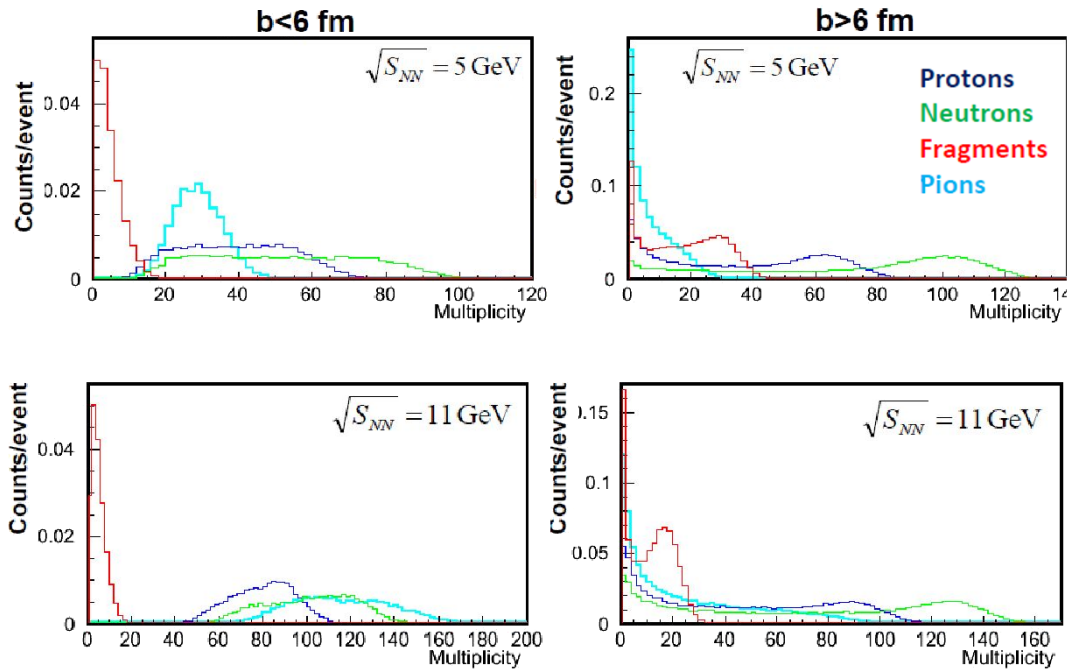
**Fig. 6:** Distribution for same types of particles as in Fig. 5 vs radial distance from the center of the FW ( $R_{FW}$ ) at the FW  $z$  position along the beam line direction for beam energies  $\sqrt{s_{NN}} = 5$  GeV (up) and  $\sqrt{s_{NN}} = 11$  GeV (down) in two event classes  $b < 6$  fm (left) and  $b > 6$  fm (right).



**Fig. 7:**  $A$ -distribution of the fragments in the FHCAL acceptance for  $Au - Au$  collisions at  $\sqrt{s_{NN}} = 5$  GeV (up) and  $\sqrt{s_{NN}} = 11$  GeV (down) in two event classes  $b < 6$  fm (left) and  $b > 6$  fm (right).



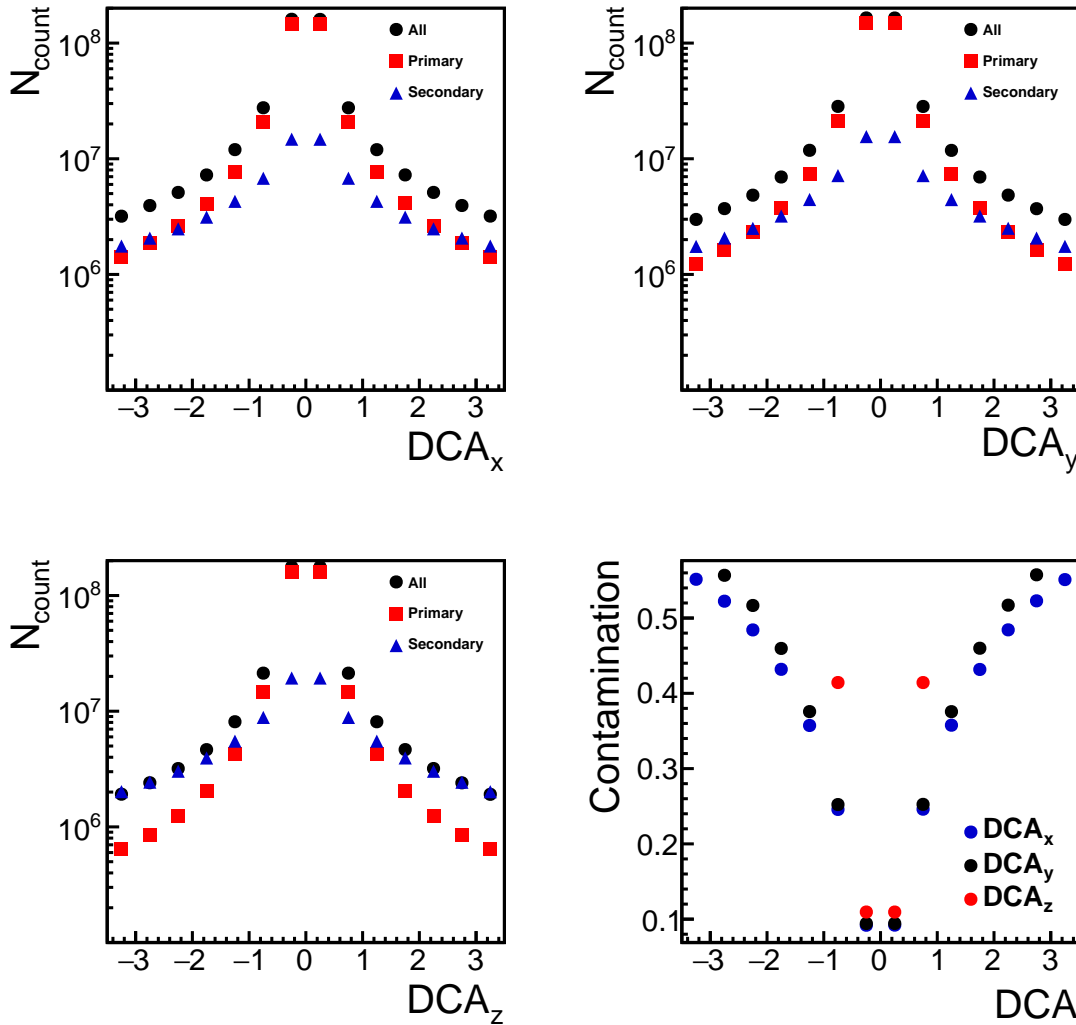
**Fig. 8:** Energy distribution for different particles in the FHCAL acceptance for  $Au - Au$  collisions at  $\sqrt{s_{NN}} = 5$  GeV (up) and  $\sqrt{s_{NN}} = 11$  GeV (down) in two event classes  $b < 6$  fm (left) and  $b > 6$  fm (right).



**Fig. 9:** Multiplicity distribution in the FHCAL acceptance for different particles at  $\sqrt{s_{NN}} = 5$  GeV (up) and  $\sqrt{s_{NN}} = 11$  GeV (down) in two event classes  $b < 6$  fm (left) and  $b > 6$  fm (right).

### 270 3.4 TPC track selection for flow analysis

271 For analysis a set of cuts to select primary tracks was developed. The secondary contamination was  
 272 estimated by using the information (*motherID* parameter) from GEANT3 about primary and secondary  
 273 tracks. For primary track selection a cut on the track's 3 dimensional distance of closest approach (DCA)  
 to the reconstructed primary vertex was used, see Fig. 10(left). Distributions of secondary tracks are



**Fig. 10:** DCA distribution for (upper left)  $x$  and  $y$  (upper right) direction. (bottom left) DCA distribution for  $z$  axis. (bottom right) Secondaries contamination. Primary and secondary tracks here were selected using the *motherID* parameter.

274 wider than that of primary tracks. A DCA cut of  $2\sigma$  reduces a fraction of secondary particles to less  
 275 than 10% as shown in Fig. 10(right). The secondary contamination is calculated as  $C_{secondaries} = 1 -$   
 276  $N_{primary}/N_{all}$ , where  $N_{primary}$  is the number of primary tracks selected by *motherID*,  $N_{all}$  is the number  
 277 of all tracks.  
 278

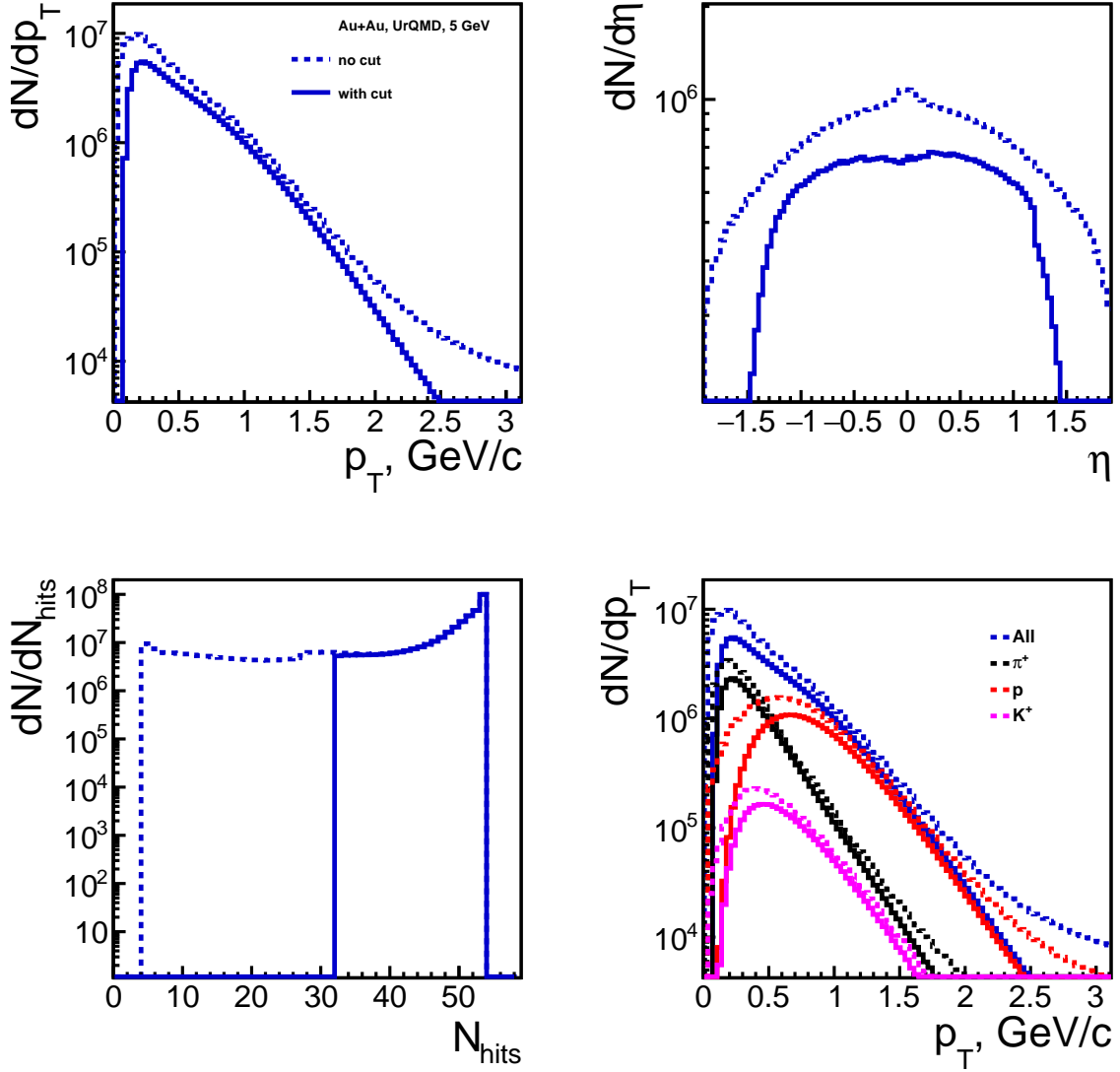
279 A set of track cuts was applied in the performance study:

280 – Number of hits associated to the TPC track:  $N_{hits} > 32$



- 281 – Track pseudorapidity:  $|\eta| < 1.5$   
 282 – Track transverse momentum:  $0 < p_T < 3 \text{ GeV}/c$   
 283 – DCA cut:  $2\sigma$

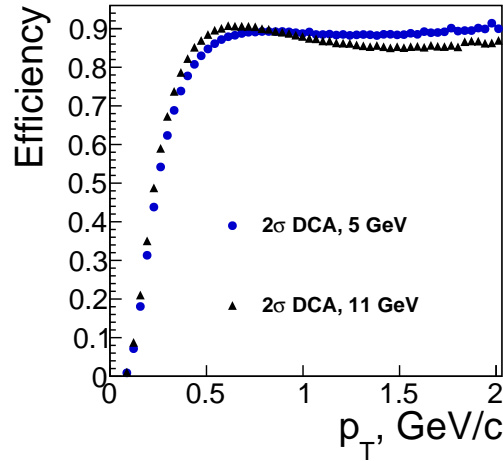
Figure 11 shows track parameter distributions before and after the track selection.



**Fig. 11:**  $p_T$  (top-left),  $\eta$  (top-right),  $N_{\text{hits}}^{TPC}$  (bottom-left) and  $p_T$  distributions for identified hadrons (bottom-right) spectra before and after track selection.

284

285 For particle identification the PDG codes from GEANT3 were used in Figures 11 and 12. Identified  
 286 charged hadrons were used for flow reconstruction. Efficiency of the reconstructed tracks as a function of  
 287 transverse momentum  $p_T$  is shown in Fig. 12. Efficiency is calculated as  $\text{eff}_{(p_T)} = (dN_{\text{reco}}/dp_T)/(dN_{\text{MC}}/dp_T)$ ,  
 288 where  $dN_{\text{reco}}/dp_T$  is the reconstructed transverse momentum yield and  $dN_{\text{MC}}/dp_T$  is the generated trans-  
 289 verse momentum yield with the UrQMD model. Figure 12 shows efficiency for protons. Results obtained  
 290 for two energies  $\sqrt{s_{NN}} = 5 \text{ GeV}$  and  $11 \text{ GeV}$  are shown. Based on  $p_T$  efficiency distribution, the follow-  
 291 ing  $p_T$  cut was applied  $p_T > 0.2 \text{ GeV}/c$ .



**Fig. 12:**  $p_T$  dependence of the reconstruction efficiency for protons from  $Au + Au$  collisions at  $\sqrt{s_{NN}} = 5$  GeV and 11 GeV.

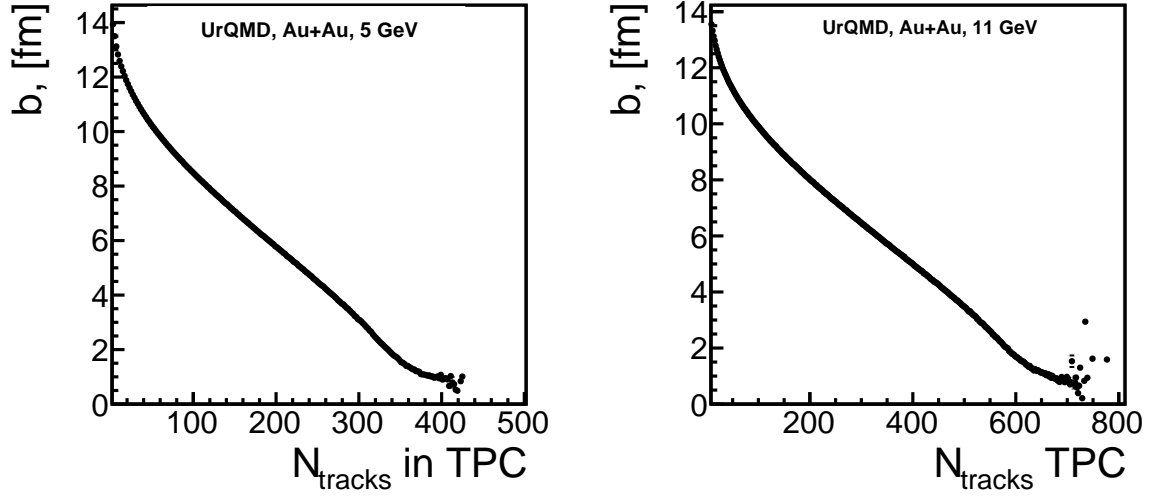
### 292 3.5 Centrality determination

293 The magnitude of the impact parameter,  $b$ , or the number of participating nucleons for a given heavy  
 294 ion collision are not known experimentally. Instead, the multiplicity of the produced particles in the  
 295 overlap zone of the nuclei is used as an experimental proxy of the  $b$  value. Since the  $b$  value and particle  
 296 multiplicity are correlated only on average, the measured multiplicity can be only used to estimate the  
 297 average impact parameter value and its spread for a given multiplicity (centrality) class of events. In  
 298 practice, all events are sorted in centrality classes. The most central class is the collisions with highest  
 299 multiplicity of the produced particles and the peripheral one is with lowest multiplicity.

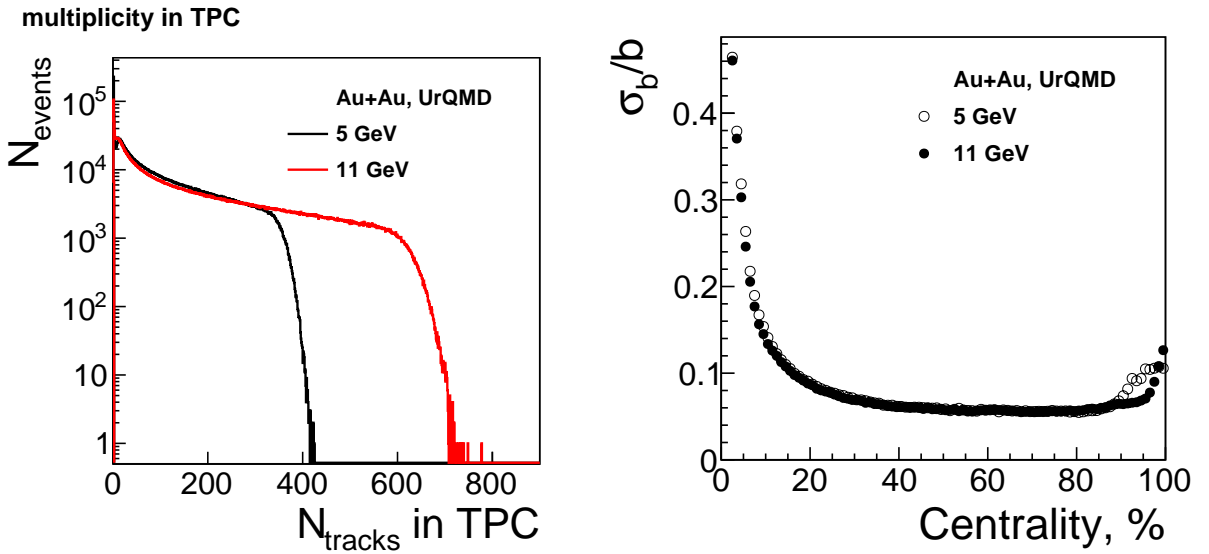
300 The multiplicity of the spectators (collision fragments) can be also used for collision centrality determi-  
 301 nation. Spectators provide an independent way to determine centrality which is important for physics  
 302 studies such as event-by-event fluctuations of various physics observables. In the case of spectator mea-  
 303 surements, the most central events correspond to a low spectator multiplicity (or a small energy deposi-  
 304 tion in the FHCAL), while peripheral events result in large amount of spectators (and typically in a large  
 305 energy deposition in the FHCAL).

#### 306 3.5.1 TPC centrality estimation

307 The impact parameter  $b$  and the particles multiplicity are well correlated (Fig. 13). One can determine  
 308 centrality from TPC multiplicity distribution Fig. 14(left) by slicing it in equal fractions of the total num-  
 309 ber of events (fraction of the total inelastic nucleus-nucleus cross section). The resulting  $\sigma_b/b$  resolution  
 310 is shown in Fig. 14(right).



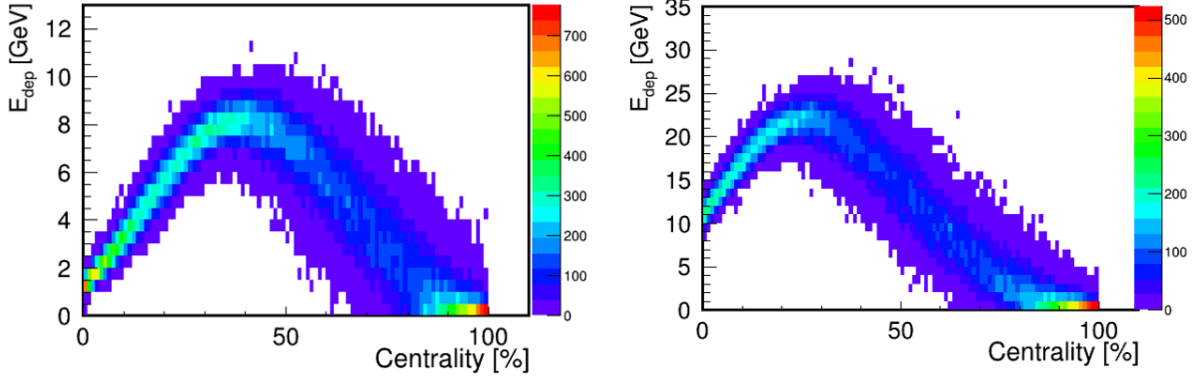
**Fig. 13:** Correlation between the impact parameter  $b$  and the TPC track multiplicity for  $Au + Au$  collisions at  $\sqrt{s_{NN}} = 5$  (left) and 11 GeV (right) simulated with the UrQMD model.



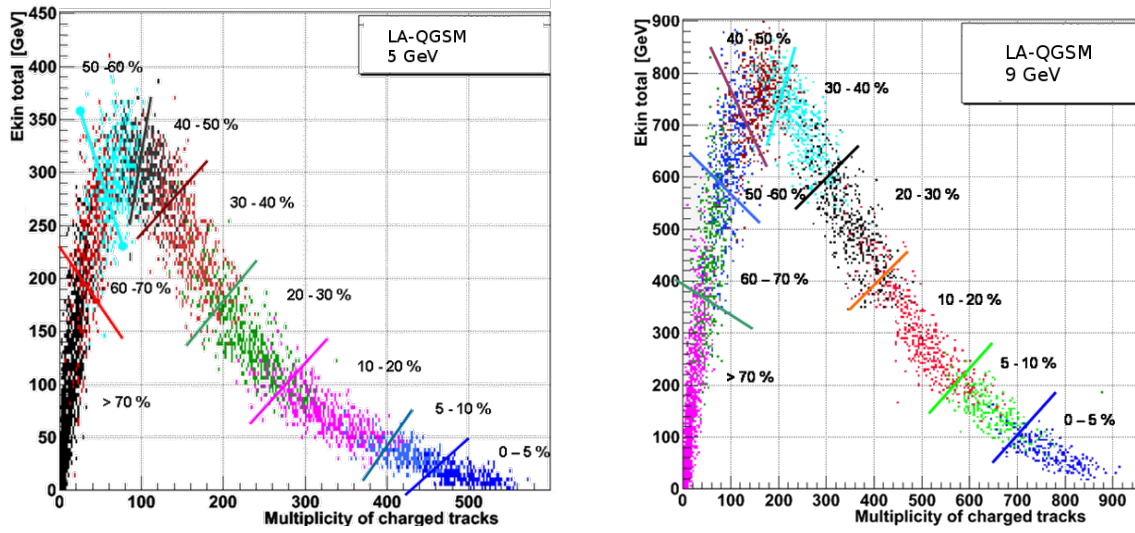
**Fig. 14:** (left) Distribution of the TPC track multiplicity. (right) Impact parameter resolution with the TPC centrality estimator. Results obtained with two versions of the MPD tracking algorithm using so-called hit producer and cluster finder are shown. See text for more details.

### 311 3.5.2 FHCAL centrality estimation using correlation with the TPC track multiplicity

312 Figure 15 shows the impact parameter dependence of the energy deposited in the FHCAL. Due to the loss  
 313 of fragments in the FHCAL beam hole the correlation is distorted for peripheral events. As a result, it is  
 314 not possible to discriminate central and peripheral collisions using FHCAL information alone. Correlation  
 315 between the FHCAL energy and TPC track multiplicity can be used to alleviate this ambiguity in a wide  
 316 centrality range (see Fig. 16).



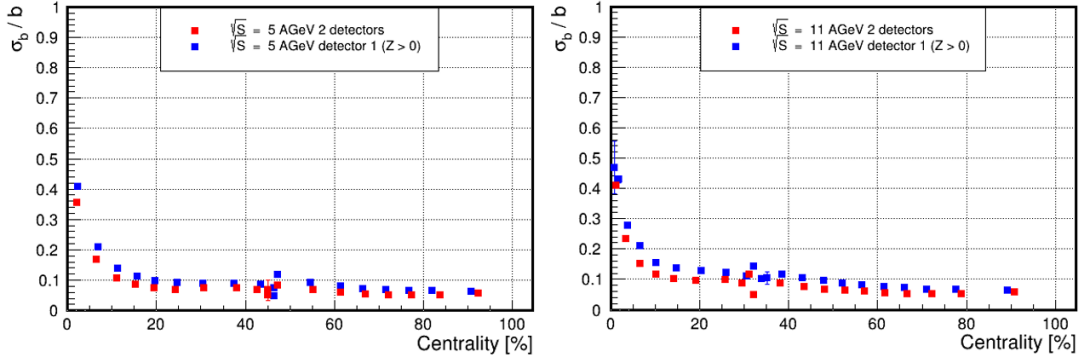
**Fig. 15:** The dependence of energy deposition in FHCAL on the centrality for the  $Au + Au$  collisions with energy  $\sqrt{s_{NN}} = 5$  GeV (left) and  $\sqrt{s_{NN}} = 11$  GeV (right).



**Fig. 16:** The correlation between energy deposition in FHCAL and charged tracks multiplicity in TPC for the  $Au + Au$  collisions with energy  $\sqrt{s_{NN}} = 5$  GeV (left) and  $\sqrt{s_{NN}} = 9$  GeV (right).

317 The resulting impact parameter resolution expressed as a ratio  $\sigma_b / \langle b \rangle$  of the width  $\sigma_b$  to mean value  $\langle b \rangle$   
 318 is shown in Fig. 17.

319 The resulting centrality resolution is below 10% for midcentral collisions. For the most central collisions,  
 320 the event-by-event fluctuations of the number of participants (and spectator energy seen by the FHCAL)  
 321 is diluting the  $b$  resolution.



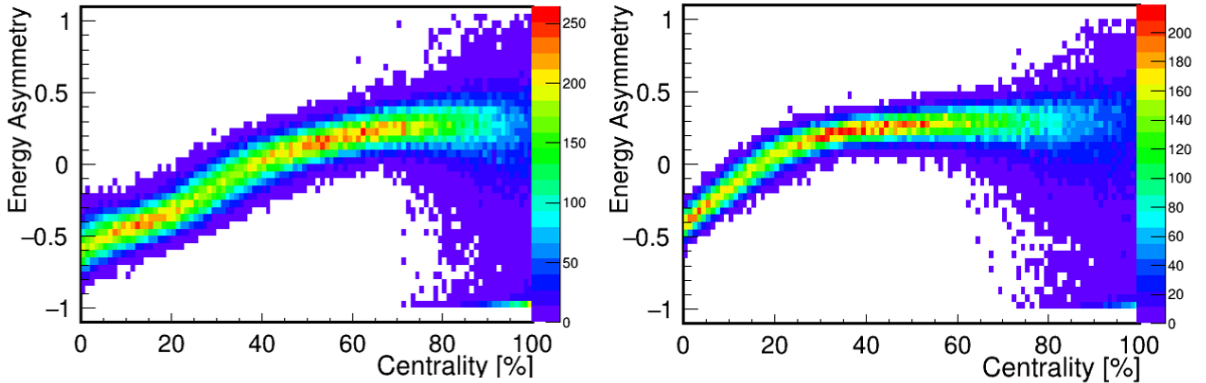
**Fig. 17:** The resolution of impact parameter obtained in separate bins of the energy depositions in FHCAL for beam energy  $\sqrt{s_{NN}} = 5$  GeV (left) and  $\sqrt{s_{NN}} = 11$  GeV (right). Blue and red points correspond to the one and two parts of FHCAL, respectively.

### 3.5.3 Centrality estimation using FHCAL-subevent energy correlation

As discussed above, the energy deposition in the FHCAL alone cannot resolve the ambiguity in the central and peripheral events (see Fig. 15). The information about the transverse profile of the energy depositions in FHCAL can be used. Clearly, that the number of the fragments that hit the FHCAL near the beam axis depends on the impact parameter. Also, the number of produced particles (mainly, pions) depends on the centrality of the collision. And the most part of the pions hit the peripheral region of FHCAL. As a sequence, the energy deposition in the central and outer regions of FHCAL must depend on the centrality. From the energy deposition in inner (outer) modules of the FHCAL  $E_{in}$  ( $E_{out}$ ) as illustrated in Fig. 4(middle) one can calculate the asymmetry,  $A_E$ :

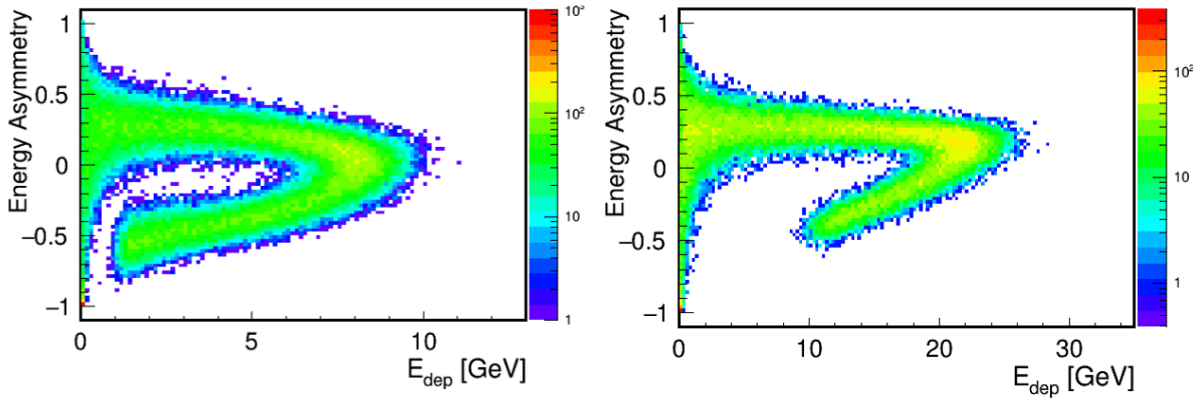
$$A_E = \frac{E_{in} - E_{out}}{E_{in} + E_{out}}, \quad (1)$$

where  $E_{in}$  and  $E_{out}$  are energy depositions in inner and outer FHCAL modules, respectively.



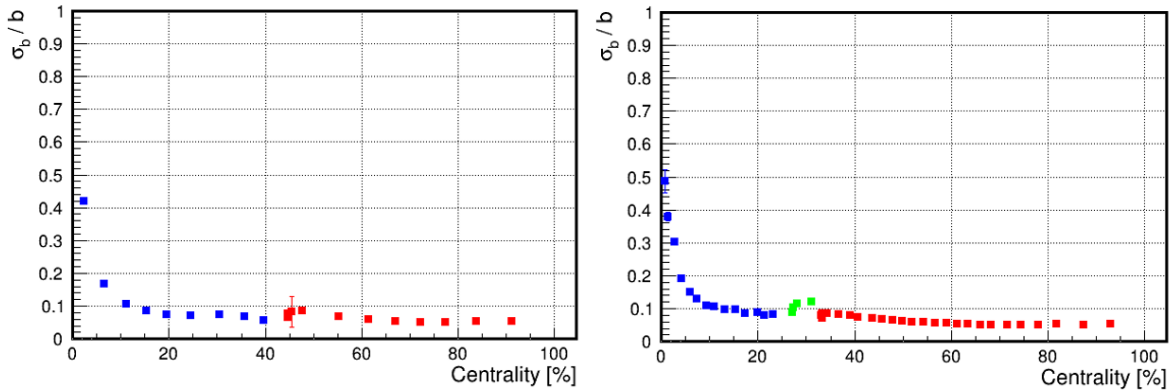
**Fig. 18:** Dependence of the energy asymmetry,  $A_E$  on impact parameter in FHCAL for  $Au + Au$  collisions at  $\sqrt{s_{NN}} = 5$  (left) and 11 GeV (right) simulated with the LA-QGSM model.

Figure 18 shows the dependence of the energy asymmetry  $A_E$  on the impact parameter for  $Au+Au$  collision at  $\sqrt{s_{NN}} = 5$  and 11 GeV. One can see, that both, energy deposition in FHCAL and asymmetry dependences are rather similar and might be used for the determination of the centralities. Unfortunately, both dependences have the ambiguity in the central and peripheral events. The correlation between the



**Fig. 19:** Correlation between the energy asymmetry,  $A_E$ , and total energy deposition,  $E_{dep}$  in FHCAL for  $Au + Au$  collisions at  $\sqrt{s_{NN}} = 5$  (left) and 11 GeV (right) simulated with the LA-QGSM model.

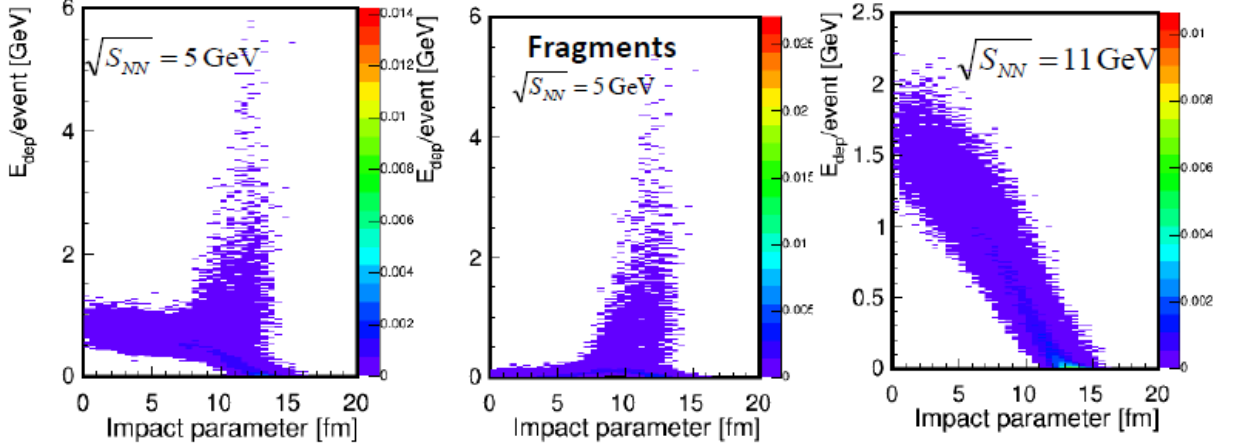
336 FHCAL energy and asymmetry  $A_E$  (Figure 19) avoids this ambiguity and can be used to differentiate the  
 337 central and peripheral events. The negative (positive) values of the  $A_E$  correspond to the central (periph-  
 338 eral) events, respectively. The corresponding impact parameter resolution is presented in Fig. 20. For  
 339 beam energy  $\sqrt{s_{NN}} = 5$  GeV blue (red) symbols corresponds to the negative (positive) values of the  $A_E$ .  
 340 The situation is slightly different for  $\sqrt{s_{NN}} = 11$  GeV. Here additional region with the  $0.1 < A_E < 0.2$  is  
 341 introduced with the corresponding green symbols, see Fig. 20, right. More complicated two-dimensional  
 342 analysis can be applied to improve the centrality selection.



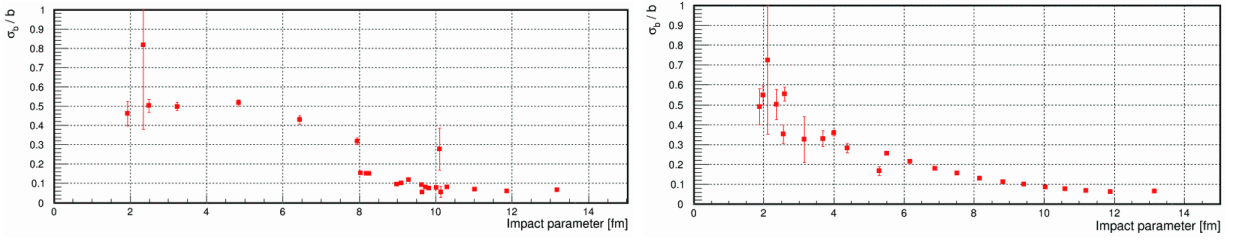
**Fig. 20:** Impact parameter resolution as a function of centrality taken in different energy deposition bins and in different regions of energy asymmetry. For  $\sqrt{s_{NN}} = 5$  GeV (left panel) the centrality bins with negative (positive)  $A_E$  values are indicated by blue (red) symbols, respectively. For  $\sqrt{s_{NN}} = 11$  GeV the centrality bins with  $A_E < 0.1$  are indicated by blue symbols, with the  $0.1 < A_E < 0.2$  - by green symbols and with  $A_E > 0.2$  - by red symbols.

### 343 3.5.4 Centrality estimation with FHCAL vs. FW

344 Performance of FW for the centrality determination was also examined. The simulated signal in the FW  
 345 vs. the impact parameter is shown Fig. 21). The energy in FW is deposited by both, charged spectators  
 346 and produced pions. The contributions of the two types of particles are different at different centralities.  
 347 The pion contribution is the largest for the central events, while the spectators prevail in the peripheral  
 348 collisions.



**Fig. 21:** Correlation between the energy deposition in FW and impact parameter for  $Au + Au$  collisions simulated with the LA-QGSM model for (left)  $\sqrt{s_{NN}} = 5$  GeV, (middle)  $\sqrt{s_{NN}} = 5$  GeV with fragments only, and (right)  $\sqrt{s_{NN}} = 11$  GeV.



**Fig. 22:** Resolution of the impact parameter with FW. (left)  $\sqrt{s_{NN}} = 5$  GeV; (right)  $\sqrt{s_{NN}} = 11$  GeV.

349 Figure 22 shows  $\sigma_b/\langle b \rangle$  calculated for FW following the same procedure as for FHCAL. The centrality  
 350 resolution of the FW is significantly worse than of the FHCAL.

### 351 3.5.5 Conclusion on centrality performance

352 Both, the TPC track multiplicity and FHCAL energy (with additional use of the correlation between the  
 353 track multiplicity and FHCAL energy or energy asymmetry in the FHCAL) can be used for centrality de-  
 354 termination. The resolution for impact parameter are comparable for TPC (Fig. 14) and FHCAL (Fig. 20)  
 355 estimators and is between 5-10% for (mid-)central collisions.

### 356 3.6 Particle identification with TPC and TOF detectors

357 The realistic particle identification is achieved by the energy loss ( $dE/dx$ ) measurements from TPC and  
 358 can be complemented by mass ( $m^2$ ) measurements using TOF. Probability vector assigned to the track is  
 359 the outcome result of the identification procedure. It denotes the probability of the track to be the certain  
 360 particle species.

### 361 **3.6.1 Identification based on the energy loss in TPC**

362 Particle species is defined by the distance between the  $dE/dx$  value from the track and the most probable  
363  $dE/dx$  value from fit function based on the simplified Bethe-Bloch equation:

$$-\frac{dE}{dx} = a_0 \left( \frac{p}{\sqrt{p^2 + m^2}} \right)^{-a_3} \left\{ a_1 - \left( \frac{p}{\sqrt{p^2 + m^2}} \right)^{a_3} - \ln \left( a_2 + \left( \frac{m}{p} \right)^{a_4} \right) \right\}, \quad (2)$$

364 which has 5 parameters  $a_i$ .

365 Truncated energy loss has an asymmetric gaussian shape. It is parameterized by asymmetric gaussian  
366 function:

$$\frac{N}{d(dE/dx)} \equiv \frac{N}{dt} = \begin{cases} A \cdot e^{-\frac{(t-\bar{t})^2}{2\sigma^2}}, & \text{for } t < \bar{t}; \\ A \cdot e^{-\frac{(t-\bar{t})^2}{2(\sigma(1+\delta))^2}}, & \text{for } t \geq \bar{t}. \end{cases} \quad (3)$$

367 This function has 4 parameters: most probable value  $\bar{t}$ , width  $\sigma$ , amplitude  $A$ , asymmetry parameter  
368  $\delta$ . Momentum  $p$  dependence of the  $\sigma$  and  $\delta$  have been parameterized by the first-order polynomial  
369 functions.

370 There are two methods to determine amplitude parameter  $A$  in (3): one can define it using momen-  
371 tum distribution fits of each particle (multiplicity method) or set it to the default value  $A = 1$  (n-sigma  
372 method).

### 373 **3.6.2 Combined identification procedure**

374 The combined identification procedure is similar to that described above, but instead of 1-dimensional  
375 distributions of  $dE/dx$  values only, there are 2-dimensional distributions of  $dE/dx$  values from TPC  
376 and  $m^2$  estimated from TOF signal. Along with asymmetric gaussian for  $dE/dx$  (3), mass square  $m^2$   
377 distribution has the gaussian shape:

$$\frac{N}{d(m^2)} \equiv \frac{N}{dt} = A \cdot e^{-\frac{(t-\bar{t})^2}{2\sigma^2}}. \quad (4)$$

378 The mean value  $\bar{t}$  is constant, widths  $\sigma$  are parameterized by second- and third-order polynomial func-  
379 tions for the different momentum  $p$  ranges. Amplitudes are defined similarly to that described above.

### 380 **3.6.3 Particle identification implementation in the analysis**

381 Generally, combined identification procedure based on both  $dE/dx$  and  $m^2$  values is used. Identification  
382 based on the TPC energy loss ( $dE/dx$ ) alone is used when the track lies in the outlier region on the  $m^2$  vs  
383  $p$  correlation plot (see Fig. 25). For the further results multiplicity method has been used. According to  
384 the reconstruction efficiency (see Fig. 12), following  $p_T$  cut was:  $0.2 < p_T < 2$  GeV/c. In this analysis,  
385 only TPC tracks with matched TOF hits were selected. The fraction of the tracks with TOF hit compared  
386 to all tracks (TOF efficiency) is shown in the Fig. 23.

387 Only positively charged particles are discussed in this analysis (see Fig. 24). Resulting  $m^2$  as a function  
388 of momentum is shown in Fig. 25. The  $m^2$  distributions for pions, kaons, and protons are shown in  
389 Figures 26 – 28. Different panels correspond to the intervals in  $p_T$  and  $\eta$  as indicated.

390 In this analysis, the track is considered as a certain particle if the corresponding probability is  $P_{\text{particle}} >$   
391 90%.



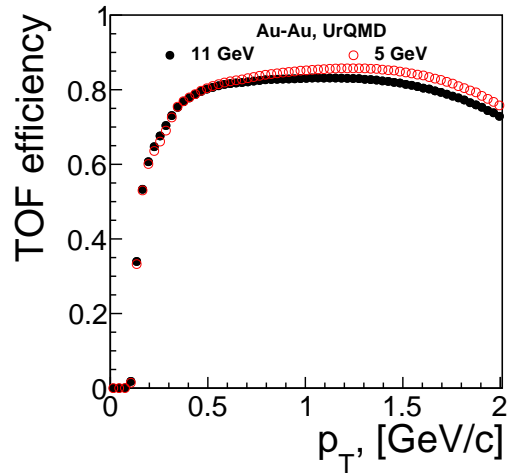


Fig. 23:  $p_T$  dependence of the TOF hit efficiency.

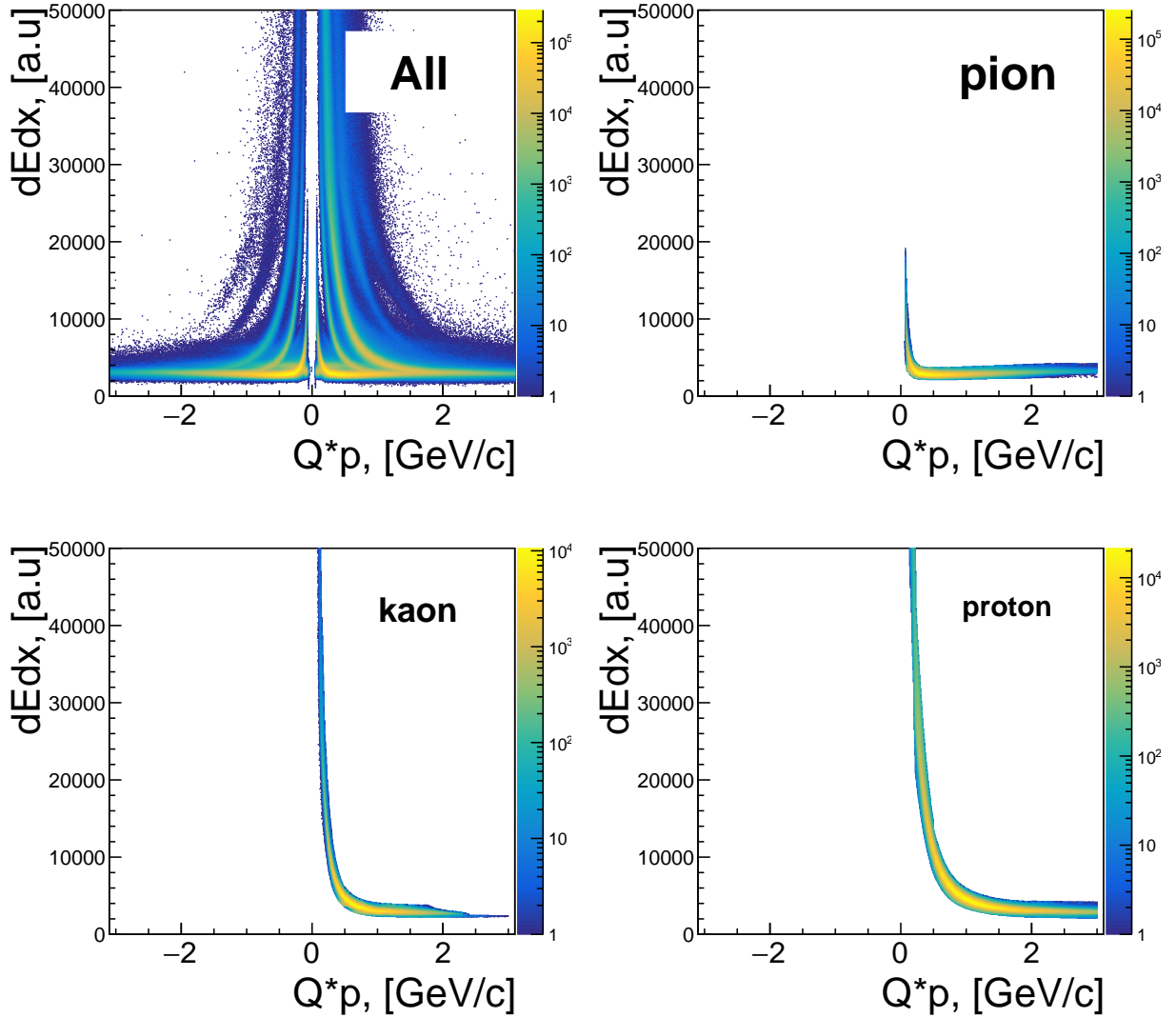
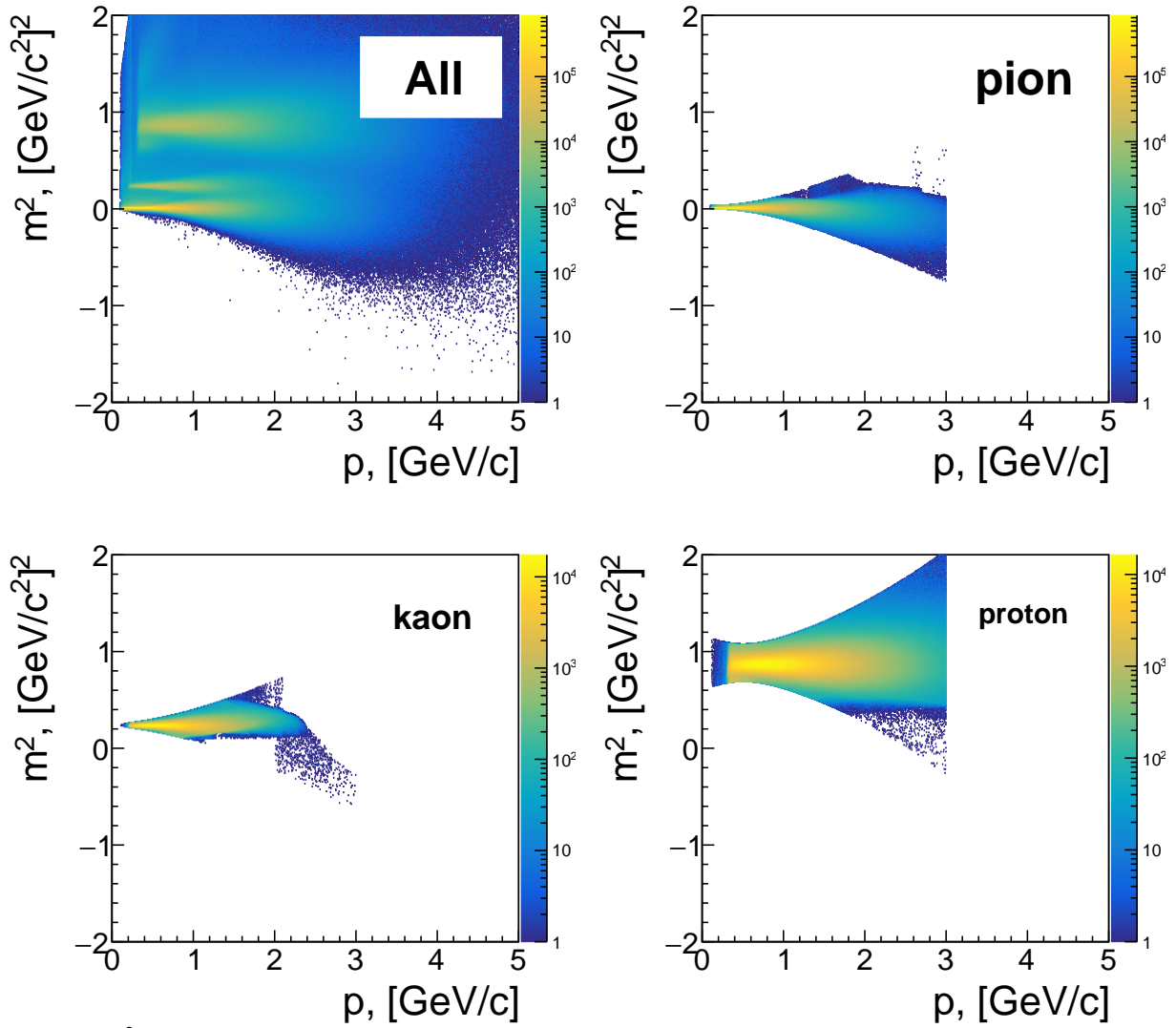
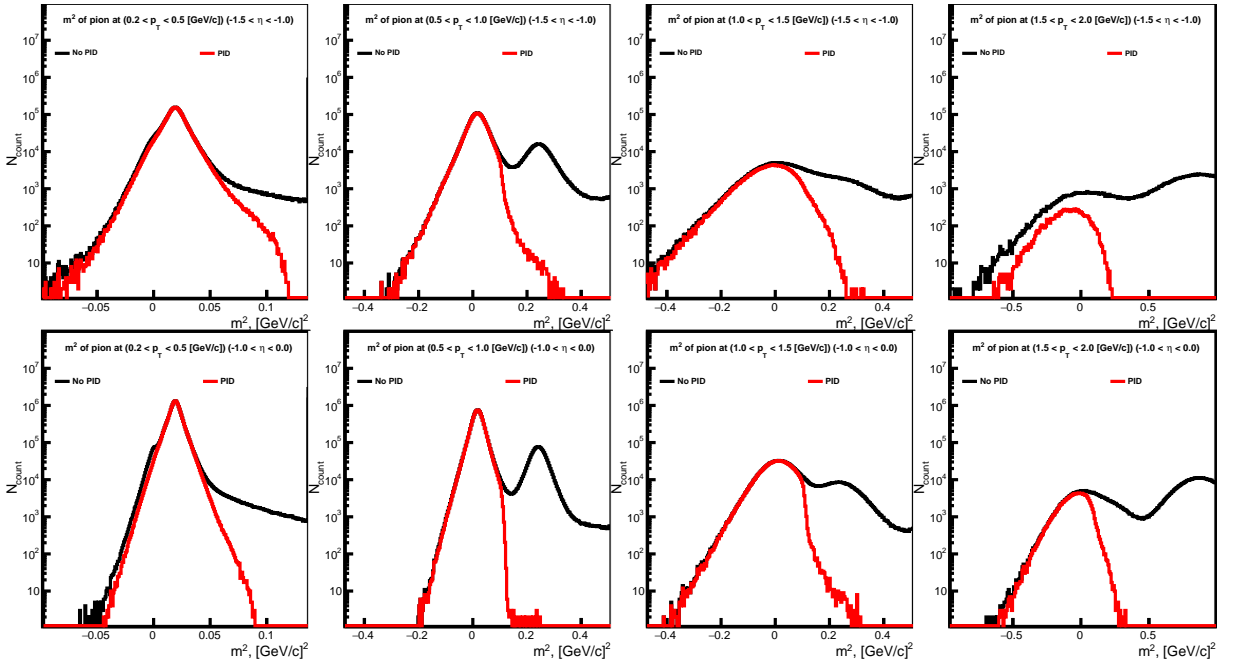


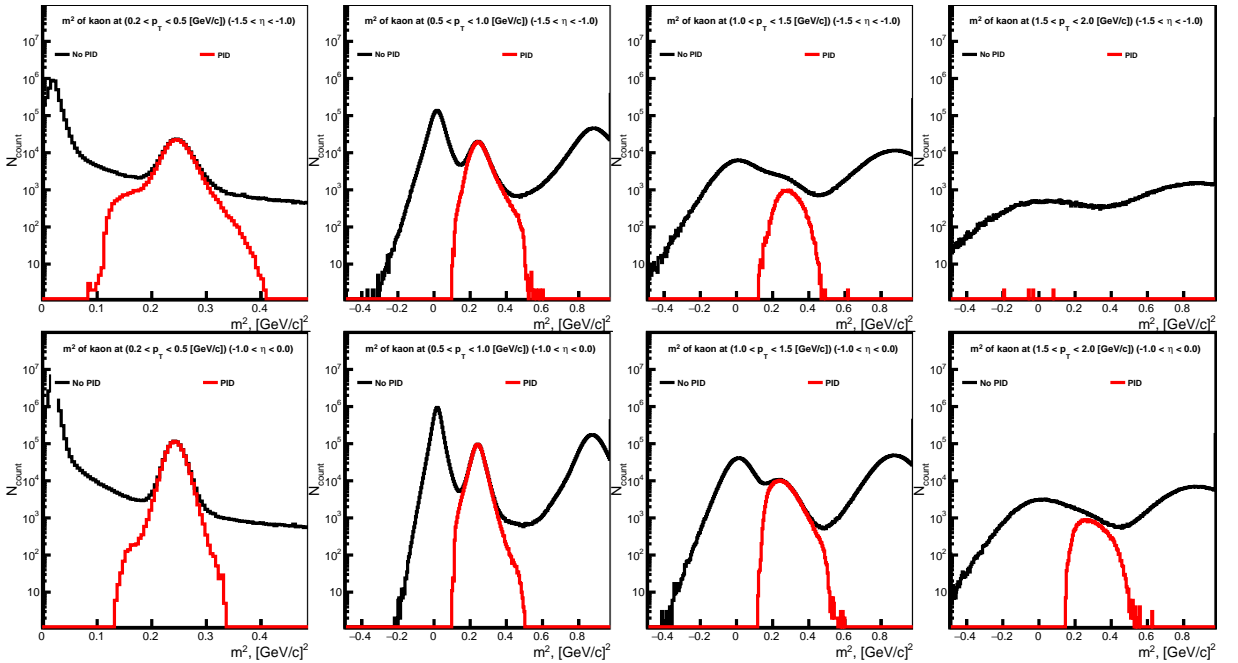
Fig. 24: Energy loss of the tracks from TPC ( $dEdx$ ) to the charged total momenta ( $Qp$ ) dependence for all particles (upper-left), pions (upper-right), kaons (bottom-left) and protons (bottom-right) tracks after selection.



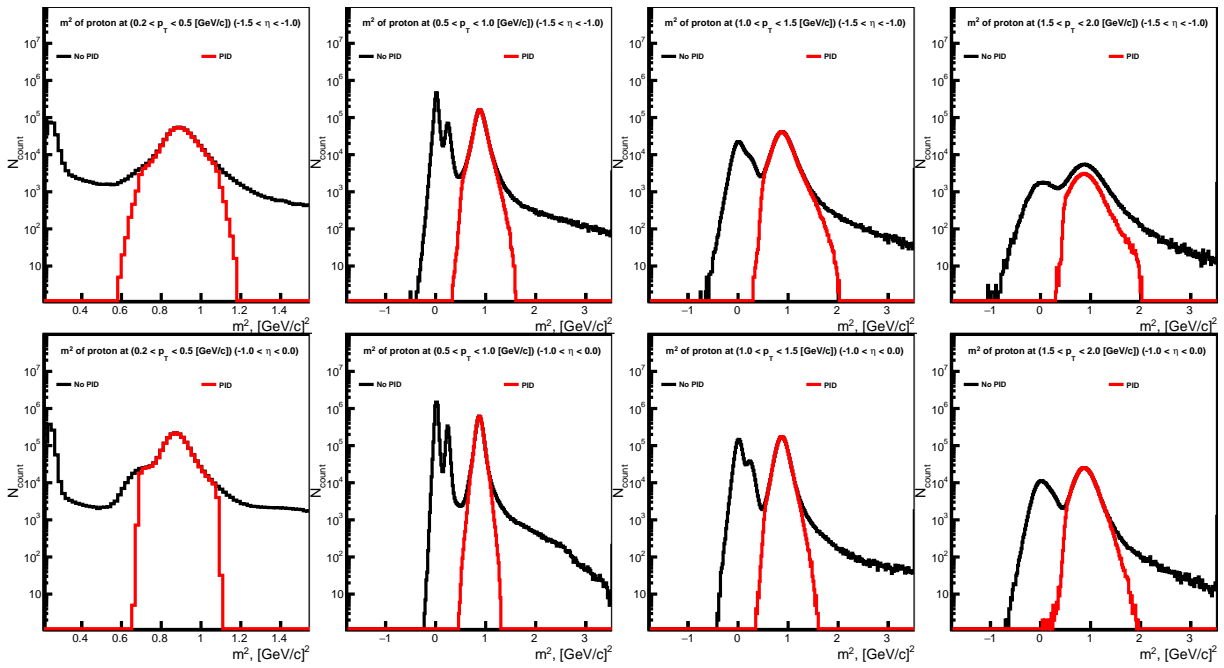
**Fig. 25:**  $m^2$  vs  $p$  dependence for all particles (upper-left), pions (upper-right), kaons (bottom-left) and protons (bottom-right) of the tracks after selection.



**Fig. 26:**  $m^2$  distributions of the positively charged particles before (black line) and after (red line) PID selection for pions ( $\pi^+$ ). Different panels correspond to the intervals in  $p_T$  and  $\eta$  as indicated.



**Fig. 27:**  $m^2$  distributions of the positively charged particles before (black line) and after (red line) PID selection for kaons ( $K^+$ ). Different panels correspond to the intervals in  $p_T$  and  $\eta$  as indicated.



**Fig. 28:**  $m^2$  distributions of the positively charged particles before (black line) and after (red line) PID selection for protons ( $p$ ). Different panels correspond to the intervals in  $p_T$  and  $\eta$  as indicated.

### 3.7 FHCAL performance for anisotropic flow measurements

#### 3.7.1 Event plane method and reaction plane resolution factor

Similar to the magnitude of the impact parameter, the reaction plane direction (or the orientation of the collision reaction plane determined by the impact parameter and the beam direction) is not known experimentally. To estimate the reaction plane orientation it is common to use the azimuthal asymmetry of particle production in the plane transverse to the beam direction.

Due to the momentum transfer between participants and spectators, the spectators (collision fragments) are deflected in the course of the collision. For non-central collisions, the asymmetry of the initial energy density in the transverse plane is aligned in the direction of the reaction plane, and the spectator deflection direction is correlated with the impact parameter (or reaction plane) direction. The plane determined by the directions of the beam and spectator deflection (spectator plane) can be used as an estimate of the reaction plane. Further, the azimuthal angle of the reaction plane in the laboratory frame is denoted as  $\Psi_{RP}$ .

The spectator deflection is experimentally accessible. It can be estimated event-by-event by utilizing the transverse segmentation and energy deposition in each of the FHCAL modules. In that respect, the FHCAL is a unique MPD detector which provides information about spectator deflection in the reaction plane. The estimated azimuthal angle of the spectator plane is called the event plane angle,  $\Psi_{1,EP}$ .

The finite number of fragments and the fluctuation of the particle multiplicity from one collision to another at fixed impact parameter orientation result in a difference between the event plane and the reaction plane orientation. This difference is usually quantified in terms of the event plane resolution (a Gaussian width of the  $(\Psi_{RP} - \Psi_{1,EP})$  distribution).

The particle azimuthal distribution relative to the reaction plane can be decomposed in a Fourier series [27]:

$$\frac{dN}{d\phi} \sim 1 + 2 \sum_n v_n \cos n(\phi - \Psi_{RP}). \quad (5)$$

Here  $\phi$  is the particle azimuthal angle and  $v_n$  are called the anisotropic transverse flow coefficients. A first few coefficients have special names, in particular the first,  $v_1$ , and second,  $v_2$ , are called the directed and elliptic flow, respectively. According to the Eq. 5, the  $v_n$  can be defined from the equation

$$v_n = \langle \cos n(\phi - \Psi_{RP}) \rangle. \quad (6)$$

where the brackets  $\langle \dots \rangle$  denote the average over all particles in a given event and over a large ensemble of events. Using the event plane angle,  $\Psi_{1,EP}$ , an experimental estimate of  $v_n$  can be obtained with the event plane method [27]

$$v_n \{ \Psi_{1,EP} \} = \frac{\langle \cos n(\phi - \Psi_{1,EP}) \rangle}{R_{1,EP}}. \quad (7)$$

The event plane resolution correction factor  $R_{1,EP}$  corrects for the finite event plane angle resolution relatively to the reaction plane and is defined as

$$R_{1,EP} = \langle \cos n(\Psi_{1,EP} - \Psi_{RP}) \rangle. \quad (8)$$

$R_{1,EP}$  value ranges between zero (very poor resolution) and unity (very good resolution). Equations (7),(8) can be used with event plane of other harmonics  $\Psi_{n,EP}$ . Directed flow  $v_1$  is large at NICA energies and is the strongest in forward rapidity region (i.e. in FHCAL acceptance area) compared to other harmonics. For this reasons the first harmonic event plane  $\Psi_{1,EP}$  is used for performance study.

Below we demonstrate the performance of the FHCAL for the event plane determination. The event plane angle is calculated from the energy deposition in a given module of the FHCAL by constructing a so-called

429 flow  $Q$ -vector [27] (two-dimensional vector in the transverse to the beam plane):

$$\vec{Q} = (Q_x, Q_y) = \left( \sum w_i \sin(\varphi_i), \sum w_i \cos(\varphi_i) \right). \quad (9)$$

430 Here  $\varphi_i$  is azimuthal angle of the center in the transverse plane of the  $i$ -th FHCAL module,  $w_i$  is a weight  
431 which is used to improve sensitivity of the event plane to the reaction plane. The weight  $w_i$  was chosen  
432 to be the energy in a given module  $i$ . The event plane angle  $\Psi_{1,EP}$  can be calculated from the  $Q$ -vector  
433 components as:

$$\Psi_{1,EP}^{L(R)} = \arctan \left( \frac{\sum E_i \sin \varphi_i}{\sum E_i \cos \varphi_i} \right), \quad \sin \varphi_i = \frac{y_i}{\sqrt{y_i^2 + x_i^2}}, \quad \cos \varphi_i = \frac{x_i}{\sqrt{y_i^2 + x_i^2}}. \quad (10)$$

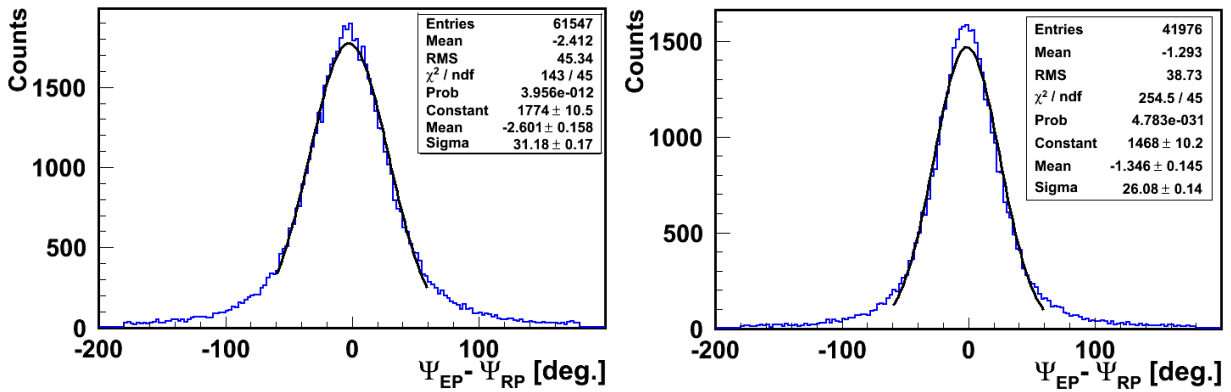
434 Here  $E_i$ ,  $x_i$  and  $y_i$  are the energy and coordinates of the  $i$ -th module, respectively. Index  $L(R)$  denotes the  
435 left (right) detectors of FHCAL.

436 The resulting event plane angle  $\Psi_{1,EP}$  is a weighted sum of the  $\Psi_{1,EP}^{L(R)}$ :

$$\Psi_{EP} = \frac{\frac{\Psi_{EP}^L}{(\sigma\Psi_{EP}^L)^2} + \frac{\Psi_{EP}^R + \pi}{(\sigma\Psi_{EP}^R)^2}}{\frac{1}{(\sigma\Psi_{EP}^L)^2} + \frac{1}{(\sigma\Psi_{EP}^R)^2}}. \quad (11)$$

### 437 3.7.2 Event plane resolution

438 The difference between the reconstructed event plane and true reaction plane reflects the angular resolution  
439 of the event plane and is shown in Fig. 29 for the beam energies  $\sqrt{s_{NN}} = 5$  and  $\sqrt{s_{NN}} = 11$  GeV.  
440 Here full setup of two calorimeter parts is used. As seen, in both cases the resolution is about 30 degree  
441 and is slightly better for the highest energy.



**Fig. 29:** The difference between the reconstructed event plane and true reaction plane for the cases of beam energy  $\sqrt{s_{NN}} = 5$  GeV (left) and  $\sqrt{s_{NN}} = 11$  GeV (right). The events with impact parameter  $b < 11$  fm are used.

442 Since the MPD detector is situated in solenoid magnetic field, it would affect the trajectories of the spec-  
443 tators (fragments) and, respectively, the precision of the event plane reconstruction. The axial solenoidal  
444 field deflects the spectators mainly in azimuthal direction and tilt the orientation of the event plane.  
445 The corresponding tilt,  $\Delta\Psi_{EP}$ , is presented in Fig. 30. It increases from  $1^\circ$  at  $\sqrt{s_{NN}} = 9$  GeV to  $3^\circ$  at  
446  $\sqrt{s_{NN}} = 3$  GeV. The calculated tilt is much smaller than the event plane resolution.

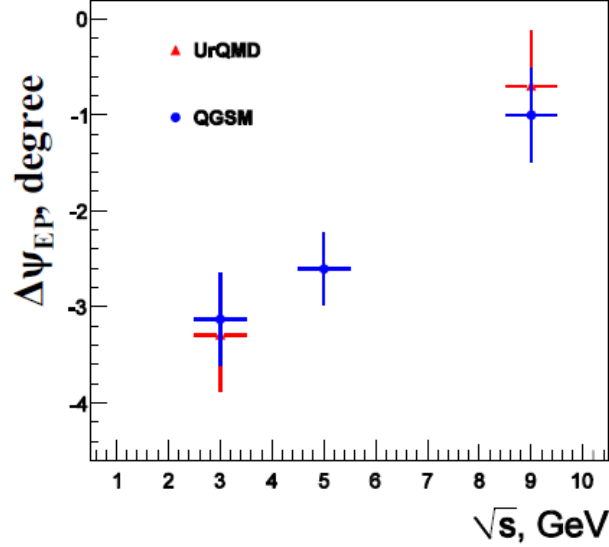


Fig. 30: The event plane angle tilt,  $\Delta\Psi_{EP}$ , caused by the solenoidal field.

447 Event plane resolution correction factor  $R_{1,EP}$  vs. centrality is presented in Fig. 31.  $R_{1,EP}$  that are given  
 448 from GEANT framework directly are called "true" and  $R_{1,EP}$  that are measured using hits from FHCAL  
 449 and particle tracks from TPC are called "reco". For the mid-central events the correction factor is as  
 450 high as 0.9. The resolution factor is estimated using energy deposition in FHCAL and different particle  
 451 generators may variate estimated centrality using multiplicity in TPC.

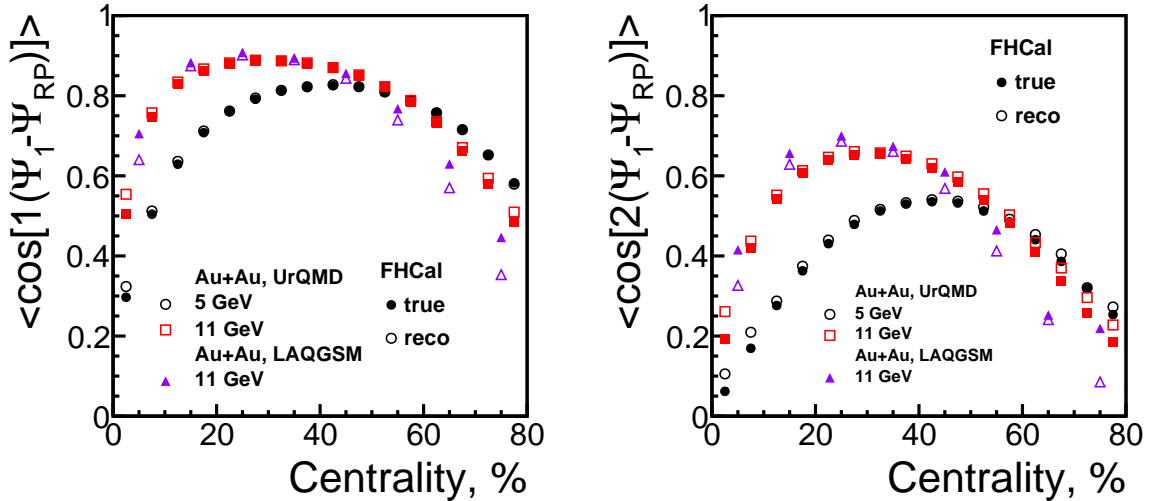


Fig. 31: Event plane resolution correction factor  $R_{1,EP}$  vs. centrality estimated with the TPC track multiplicity for the 1st (left) and 2nd (right) harmonics. Open (solid) symbols correspond to the results obtained with respect to the FHCAL event (reaction) plane. The results for different  $\sqrt{s_{NN}}=5$  (11) GeV are produced using cluster finder tracking algorithm.

452 Two event generators (LA-QGSM and UrQMD) were used to evaluate the effect of collision fragments  
 453 on the event plane resolution. Figure 32(left) shows that both generators provide similar results. The  
 454 event plane resolution degrades at beam energies  $\sqrt{s_{NN}} = 3$  GeV to about 40°. Figure 32(right) presents  
 455 the result for highFHCAL and FHCAL. The parameters of both calorimeters are practically identical at the

456 same beam energies.

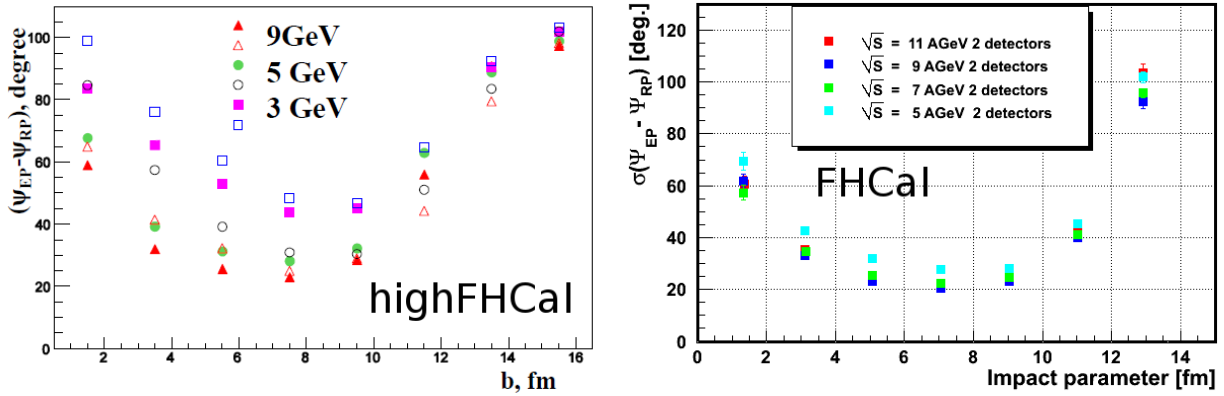


Fig. 32: The event plane resolution  $\sigma(\Psi_{RP} - \Psi_{1,EP})$  vs. impact parameter at different energies. (Left) UrQMD (Open) vs. LA-QGSM (solid) comparison for highFHCaI. (Right) Results for FHCaI.

457 Also, the event plane resolution was calculated for the Forward Wall (FW) option, that detects the charged  
 458 particles only. In case of the minimum ionizing particles (MIPs) the hit weights  $w_i$  in Eq. (9) are set to  
 459 unity. If the particles have different  $Z$  then the weight might correspond to the energy deposition in the  
 460 detector.

461 Below two sets of simulation results are presented. First is for the spectators only and the second one  
 462 is for all detected particles including the pions. The dependences of the event plane resolution on the  
 463 impact parameter are shown in Fig. 33. If only the charged spectators are used, the event plane resolution  
 464 is about  $35^\circ - 40^\circ$ , which is about 2 times lower than for the FHCaI.

465 This is natural because FW does not detect the neutrons, i.e. more than half of the spectators. The  
 466 situation is dramatically worse for the case when all charged particles, including pions, are used (see  
 467 Fig. 33(right)). The event plane resolution degrades down to  $55^\circ - 60^\circ$  for the lowest beam energies and  
 468 is extremely poor at the highest energy, where the fraction of the detected pions is comparable with that  
 469 of protons.

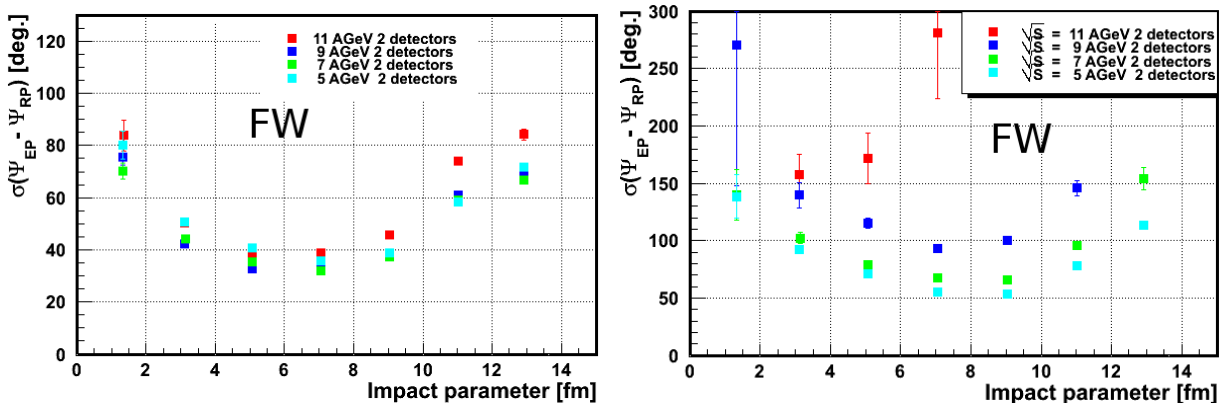
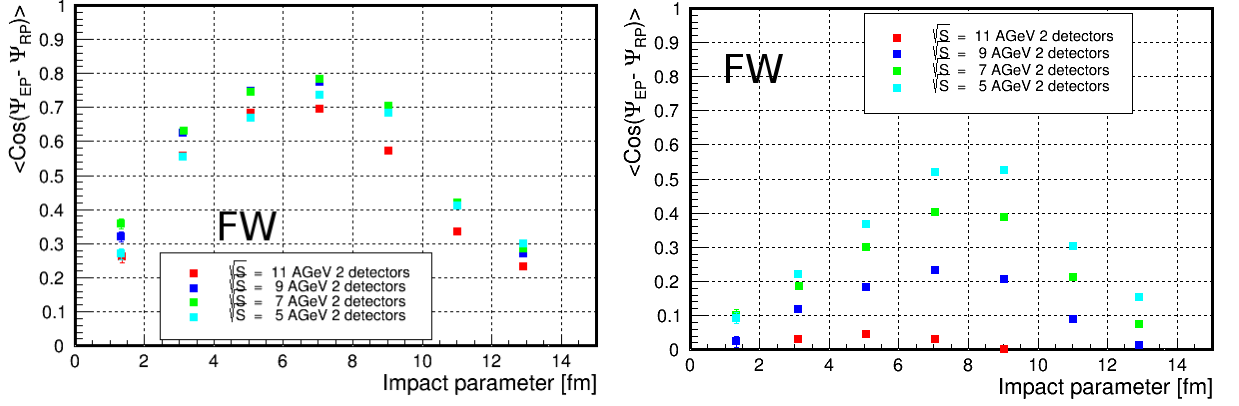


Fig. 33: The event plane resolution  $\sigma(\Psi_{RP} - \Psi_{1,EP})$  for a few beam energies for FW. Left – only charged spectators (protons and fragments) are taken in analysis, right – all detected charged particles (including pions) are included.



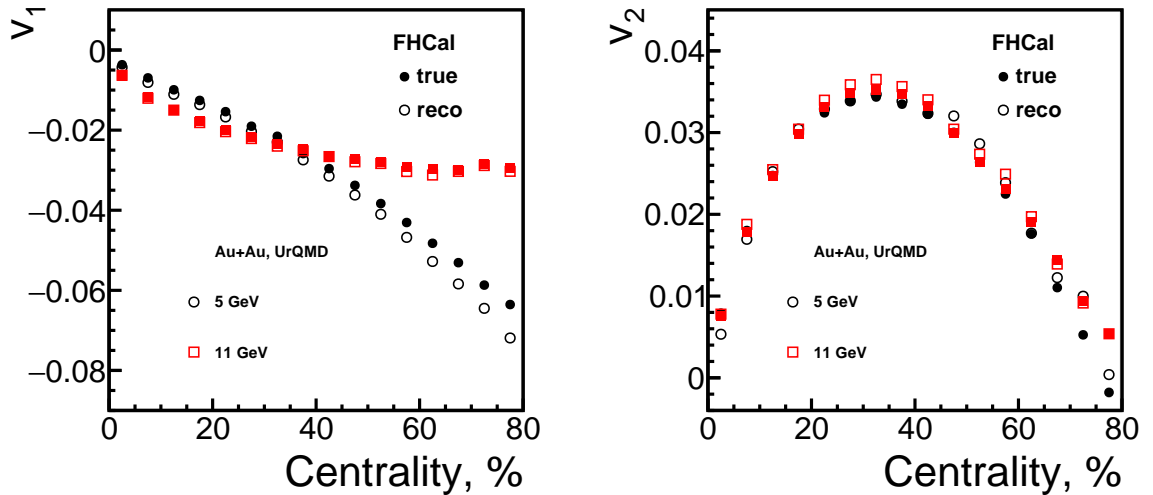
470 The corresponding event plane resolution correction factors  $R_{1,EP}$  as a function of the centrality are shown  
 471 in Fig. 34. The correction factors for the detected charged spectators are at maximum about 0.7 – 0.8,  
 472 which should be compared with a value of 0.9 for FHCaI. And again the situation is significantly worse  
 473 if all charged particles are used, see Fig. 34(right).



**Fig. 34:** The event plane resolution correction factor  $R_{1,EP}$  for FW at different collision energies. Results obtained with (left) only charged spectators (protons and fragments), (right) with all charged particles, including pions.

### 474 3.8 Performance for directed and elliptic flow of pions, kaons, and protons

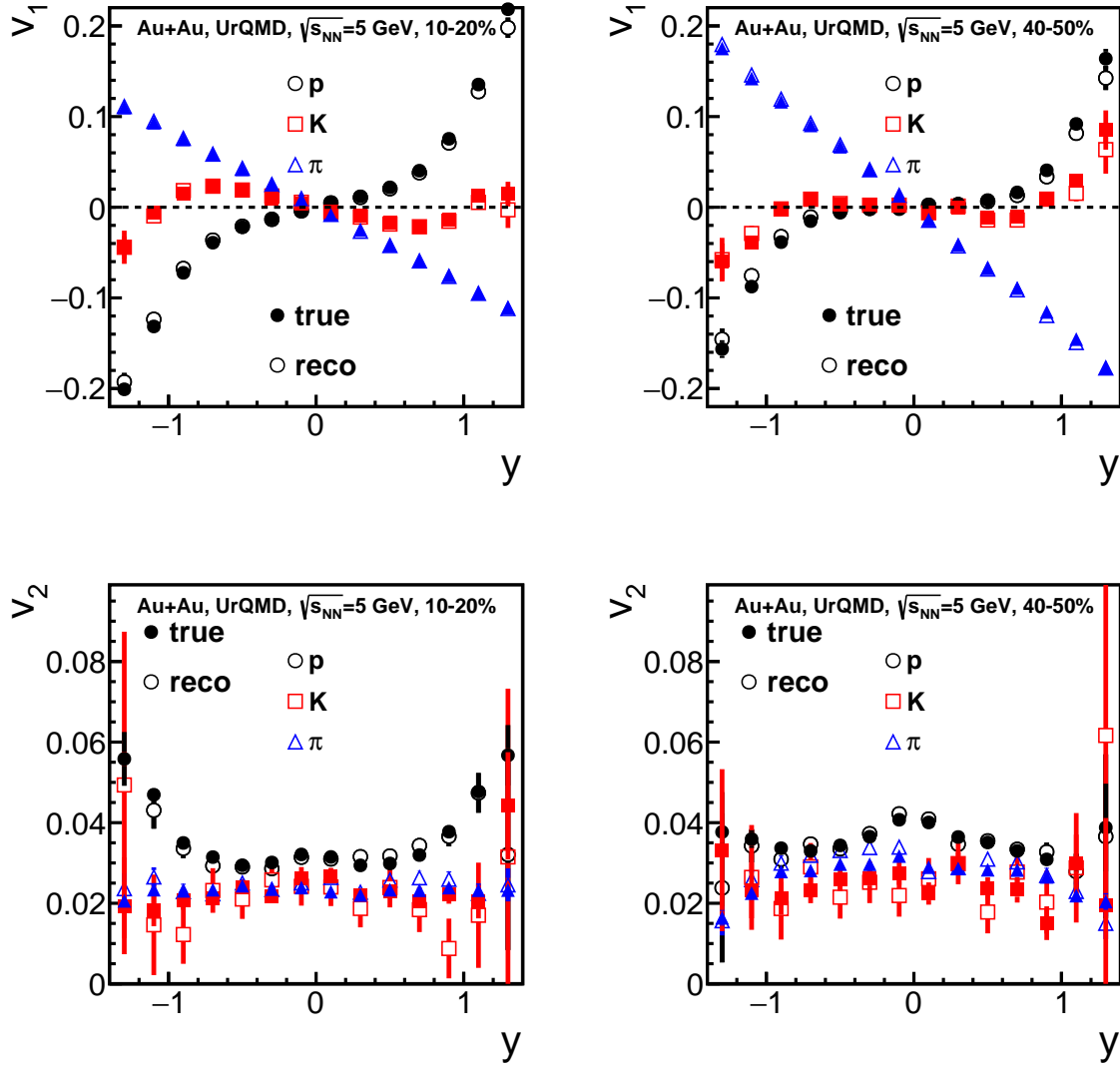
475 The centrality dependence of directed ( $v_1$ ) and elliptic ( $v_2$ ) flow of charged hadrons is presented in  
 476 Fig. 35. The open (close) symbols correspond to the reconstructed (reaction plane)  $v_n$  values.  
 Note, that reconstructed  $v_n$  for the higher energy  $\sqrt{s_{NN}} = 11$  GeV show better agreement for peripheral



**Fig. 35:** Charged particle directed (left) and elliptic (right) anisotropic flow as a function of centrality for range of  $p_T=0.2-3$  GeV and  $|\eta| < 1.5$ . Open (solid) symbols correspond to the results obtained with respect to the FHCaI event (reaction) plane.

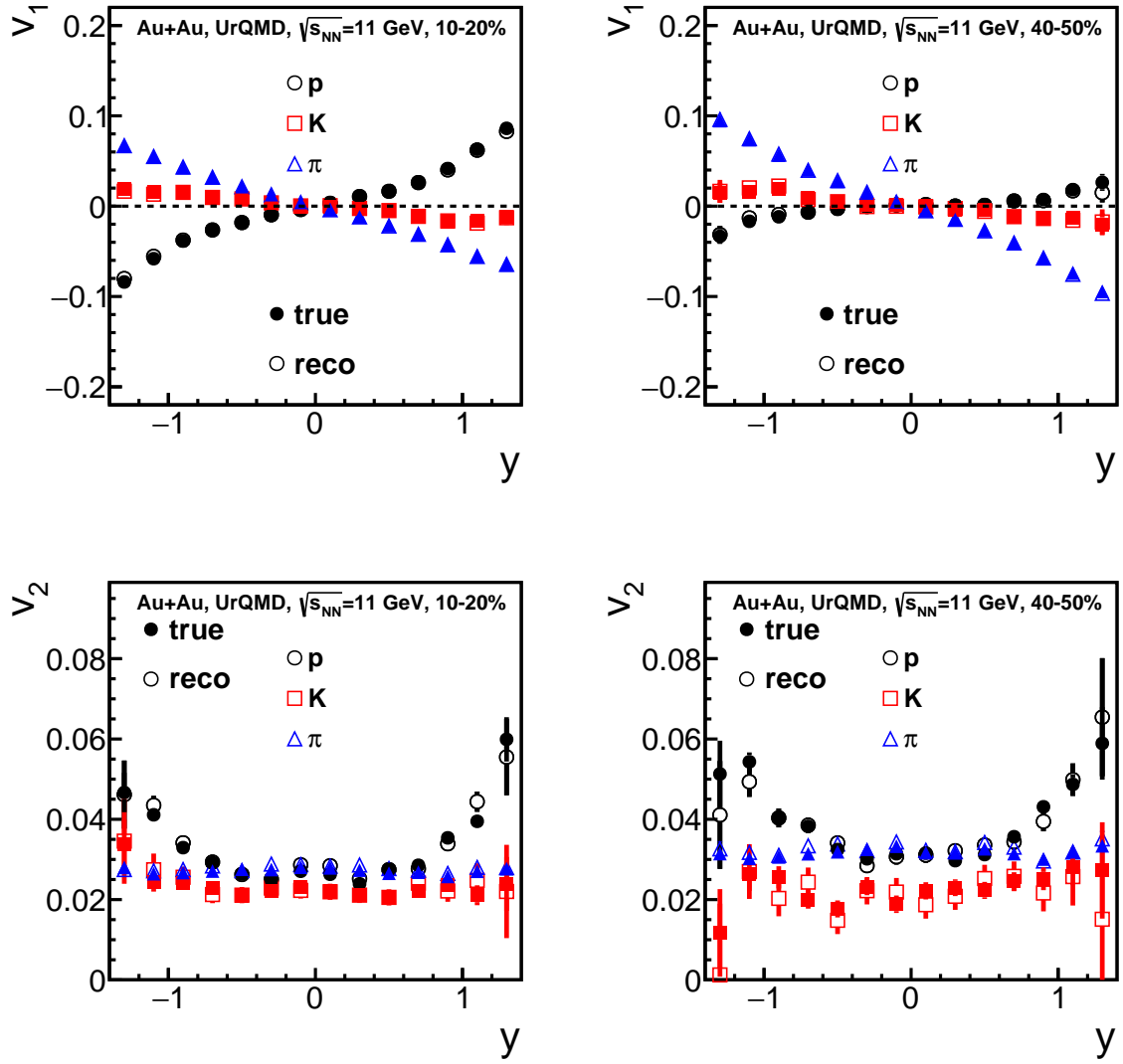
477 collisions with simulated values of  $v_n$  compared to the results for the  $\sqrt{s_{NN}} = 11$  GeV. The efficiency  
 478 correction for  $v_n$  as a function of both  $p_T$  and rapidity is needed to correct for this effect. This goes  
 479

480 beyond the scope of this documents and is a good subject of further studies. The  $v_1$  and  $v_2$  for identified  
 481 hadrons as a function of rapidity  $y$  are presented in Fig. 36 and 37, respectively.

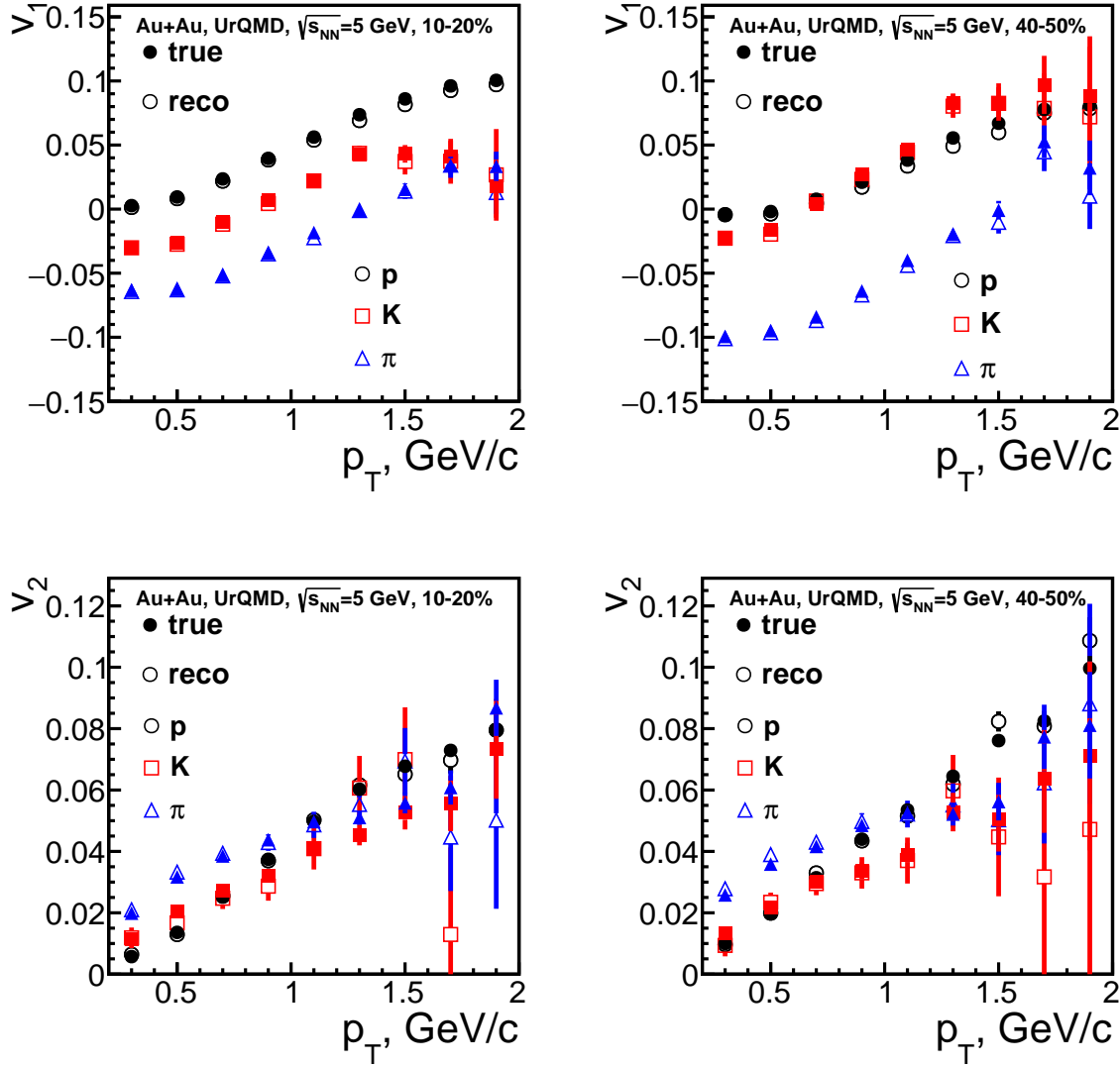


**Fig. 36:** Rapidity dependence of directed (top) and elliptic (down) flow for identified charged hadrons with  $p_T = 0.2 - 3$  GeV/c from 10–20% (left panels) and 40–50% (right panels) central Au+Au collisions at  $\sqrt{s_{NN}} = 5$  GeV. Open (solid) symbols correspond to the results obtained with respect to the FHCAL event (reaction) plane.

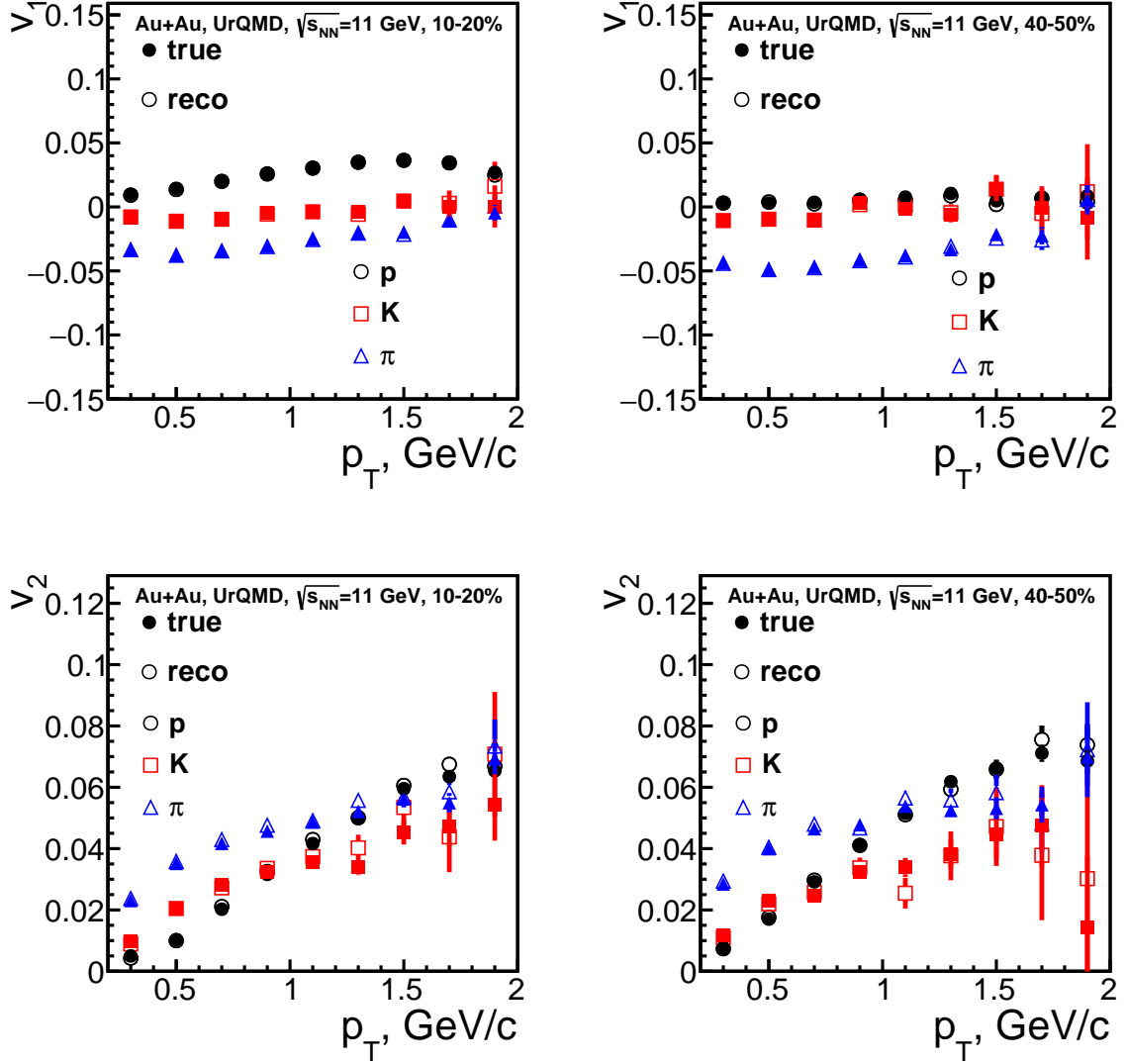
482 The  $v_1$  and  $v_2$  for identified hadrons as a function of transverse momentum  $p_T$  are presented in Fig. 38,39.



**Fig. 37:** Rapidity dependence of directed (top) and elliptic (down) flow for identified charged hadrons with  $p_T = 0.2 - 3$  GeV/c from 10 – 20% (left panels) and 40 – 50% (right panels) central  $Au + Au$  collisions at  $\sqrt{s_{NN}} = 11$  GeV. Open (solid) symbols correspond to the results obtained with respect to the FHCAL event (reaction) plane.



**Fig. 38:** Transverse momentum dependence of directed (top) and elliptic (down) flow for identified charged hadrons with  $|\eta|=0.2-1.5$  (top) and  $|\eta| < 1.5$  (down) from 10 – 20% (left panels) and 40 – 50% (right panels) central Au + Au collisions at  $\sqrt{s_{NN}} = 5$  GeV. Open (solid) symbols correspond to the results obtained with respect to the FHCAL event (reaction) plane.



**Fig. 39:** Transverse momentum dependence of directed (top) and elliptic (down) flow for identified charged hadrons with  $|\eta|=0.2-1.5$  (top) and  $|\eta| < 1.5$  (down) from 10 – 20% (left panels) and 40 – 50% (right panels) central Au+Au collisions at  $\sqrt{s_{NN}} = 11$  GeV. Open (solid) symbols correspond to the results obtained with respect to the FHCAL event (reaction) plane.

### 483 **3.9 Conclusion on anisotropic flow performance**

484 Event plane resolution expressed in terms of the correction factor  $R_{1,EP}$  for FHCAL (Fig. 31) is comparable  
485 to that of FW detector configuration (Fig. 34) which is a proxy for the ideal forward detector. This  
486 demonstrates that reaction plane resolution close to that of ideal forward detector is achieved with the  
487 current FHCAL configuration.

488 Using the event plane method and the reaction plane estimated with the FHCAL the simulated values  
489 of anisotropic flow coefficients of pions, kaons, and protons are recovered as a function of transverse  
490 momentum and rapidity in centrality classes for different collision energies (see Figures 35 and 37 –  
491 39).

## 492 **4 Technical design of the FHCAL modules**

### 493 **4.1 General consideration**

494 Initially, the design of the lead/scintillator sandwich calorimeter with WLS-fiber light readout was de-  
495 veloped a few years ago for the beam energies from 1 GeV to 30 GeV. The main requirements to the  
496 calorimeter are:

- 497 1. Modular structure adjustable for the calorimeters with the different geometries;
- 498 2. Transverse segmentation of the calorimeter with good space resolution;
- 499 3. Ability to work in strong magnetic fields;
- 500 4. Good energy resolution, close to the best values of existing hadron calorimeters;
- 501 5. Detection of the hadrons with low energies;
- 502 6. Reliable detection of low energy depositions, comparable to that from the minimum ionizing par-  
503 ticles;
- 504 7. Longitudinal segmentation to compensate the non-uniformity of the light collection along the mod-  
505 ules;
- 506 8. Compact and cheap photodetectors with high gain and low noise;
- 507 9. Possibility to calibrate with the cosmic muons.

508 Certainly, the above requirements are valid for the FHCAL at MPD which is intended for the measurements  
509 of the centrality and the reaction plane.

510 The simulation results presented in previous chapters show the appropriate performance of the calorime-  
511 ter with the proposed design. It was proved that the modular calorimeter ensures nice reconstruction  
512 of the event plane and centrality due to the transverse segmentation and good energy resolution. Nev-  
513 ertheless, it would be valuable to understand the effect of the FHCAL energy resolution at the measured  
514 parameters. Here we will consider it in details.

515 There are three main components in the energy resolution of the calorimeter: stochastic term, noise term  
516 and constant term. Noise term is the most critical for the measurements at low energies. However, let us  
517 consider first the stochastic term, which is mainly determined by two factors: the sampling fraction of  
518 the calorimeter (relative energy depositions in the absorbers and scintillators) and by the fluctuations of  
519 the photoelectrons statistics.

#### 520 **Stochastic term (sampling fraction).**

521 In present design the energy resolution of FHCAL is about  $\frac{\sigma_E}{E} \sim \frac{55\%}{\sqrt{E(\text{GeV})}}$  which is very good number  
522 for the hadron calorimeters. For example, the most hadron calorimeters have the energy resolution in  
523 the range  $\frac{(50-120)\%}{\sqrt{E(\text{GeV})}}$  (excluding some exotic cases with uranium absorbers, where the stochastic term  
524 achieves 35%). As seen, FHCAL has the resolution very close to the lowest limit. The stochastic term  
525 can be reduced by using more segmented calorimeter. Taking two times finer sampling (lead 8 mm and  
526 scintillator 2 mm thicknesses) the resolution could be improved to  $\frac{47\%}{\sqrt{E(\text{GeV})}}$  (see future ILC project, [9]).

527 This improvement in the resolution would cost two times more scintillator plates, WLS-fibers and readout  
528 channels. In addition, small thickness of the scintillator plates results in worse light collection efficiency.  
529 According to above reference, the light yield of finely segmented calorimeter is 83 photoelectrons/GeV.

530 This is almost three times lower than in present version of FHCAL (see explanation below). Meanwhile,  
531 the light yield is the principal parameter for the detection of the low energies, where the contribution of  
532 the electronic noise is essential.

533 For the reaction plane measurements, the transverse segmentation of the calorimeter is the most impor-  
534 tant issue. As shown above, the modules with  $15 \times 15 \text{ cm}^2$  transverse sizes provide the same angular  
535 resolution of the reaction plane as  $10 \times 10 \text{ cm}^2$  modules. This is a natural result, because the transverse  
536 sizes (as well as the length) of the hadronic cascade are determined by the interaction length, which is 17  
537 cm for the lead. Note, that the most of hadron calorimeters have the module sizes around  $20 \times 20 \text{ cm}^2$  to  
538 minimize the number of readout channels.

#### 539 **Stochastic term (photoelectrons statistics).**

540 Photoelectrons statistics is another important factor that has an influence at the energy resolution. This  
541 factor is especially important for the detection of the low energies, where the Poisson fluctuations of  
542 the signal might be principal. For this reason, the light readout in FHCAL modules was provided in  
543 the most sophisticated way by WLS-fibers glued in the grooves in each scintillator plate. This approach  
544 ensures the highest light yield ever achieved in hadron calorimeters. As shown below, the light yield  
545 is about 40-50 photoelectrons for the 5 MeV deposited energy in a single longitudinal section. 1 GeV  
546 proton deposits in FHCAL module about 25 MeV visible energy that corresponds to the signal of about  
547 200 photoelectrons. According to Poisson distribution, this signal has a fluctuation around 7% that is  
548 negligibly small comparing to the stochastic term of 55-60%. The comparable (three times worse) light  
549 yield was obtained in the calorimeter prototypes developed for future ILC projects, where the detection  
550 of low energy hadrons is planned.

#### 551 **Noise term in energy resolution.**

552 Noise term is especially important for the detection of low energies, where the signal amplitude might  
553 be compared with the electronic noise. There are two factors to suppress this noise. First, the use  
554 of the photodetectors and electronics with the minimum noise and second, to increase the minimum  
555 signal above the electronic noise. In FHCAL both approaches are used. The photodetectors (silicon  
556 photomultipliers) have high gain and low intrinsic noise at the level of a very few photoelectrons. From  
557 the other side, the minimum signal is about 40 photoelectrons in one longitudinal section for the MIP  
558 particle. Therefore, the minimum signal exceeds the possible electronic noise for a one order. Note,  
559 that 300 MeV protons deposit in FHCAL module about 6 MeV visible energy or above 50 photoelectrons  
560 signal. This energy might be regarded as a threshold energy for FHCAL module.

## 561 **4.2 Structure of FHCAL modules**

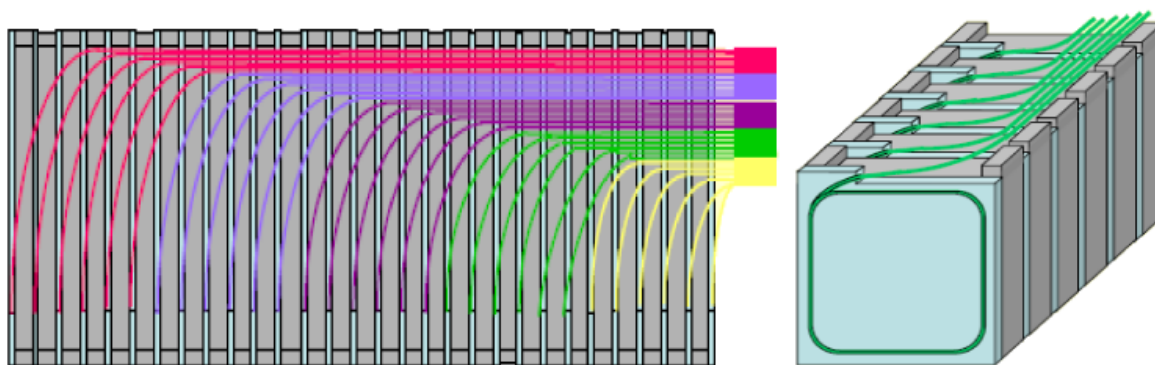
562 The structure of proposed for FHCAL modules is shown in Fig. 40. Each module of hadron calorimeter  
563 consists of 42 lead-scintillator tile sandwiches with the sampling ratio 4 : 1 (thickness of the lead plates  
564 and scintillator tiles are 16 and 4 mm, respectively) that satisfies the compensation condition.

565 Proposed scheme of the FHCAL module prototype and the light readout is shown in Fig. 40.

566 Light readout is provided by the WLS-fibers embedded in the grooves in scintillator plates that ensures  
567 high efficiency and uniformity of light collection over the scintillator tile within a very few percent.  
568 WLS-fibers from each 6 consecutive scintillator tiles are collected together and viewed by a single pho-  
569 todetector at the end of the module. The longitudinal segmentation in 7 sections ensures the uniformity  
570 of the light collection along the module. The individual calibration of longitudinal sections is essential  
571 for the monitoring of the light yield behavior. Longitudinal segmentation of the calorimeter provides  
572 also a unique opportunity to improve the energy resolution based on the measurement of the longitudinal  
573 hadron shower profile with the off-line compensating algorithm.

574 Longitudinal segmentation of the calorimeter modules requires 7 compact photodetectors coupled to the





**Fig. 40:** Scheme of the FHCAL module and light readout from scintillator tiles in FHCAL module. Left – top view (only part of the module is shown), right – front view. Fibers from each consecutive 6 tiles are collected together and viewed by a single MAPD.

575 end of WLS-fibers at the rear side of the module. The use of micropixel avalanche photodiodes, MAPDs  
 576 (or silicon photomultipliers, SiPMs) seems to be an optimum choice due to their remarkable properties  
 577 as high internal gain, compactness, low cost and immunity to the nuclear counter effect and magnetic  
 578 field.

### 579 4.3 Scintillator tiles and WLS fibers

580 The scintillator tiles with 4 mm thickness were made of polystyrene based scintillator at Vladimir plant,  
 581 Russia. They have 2 mm depth groove at the surface of the scintillator plate (Fig. 41), where the WLS  
 582 fiber is glued by the optical glue EJ-500. Each scintillator tile is covered by white reflector (TYVEK  
 583 paper) to improve the light collection. The shape of the grooves provides parallel exit of WLS fiber from  
 584 the groove relative to the upper side of the scintillator. WLS fibers Y-11(200) with double cladding and  
 585 diameter 1 mm produced by Kuraray Co. were used for the FHCAL assembling. The light attenuation  
 586 length of this fiber is about 4.5 m [28]. To avoid the loss of the light the bending radius of the WLS fiber  
 587 must be larger than 5 cm.

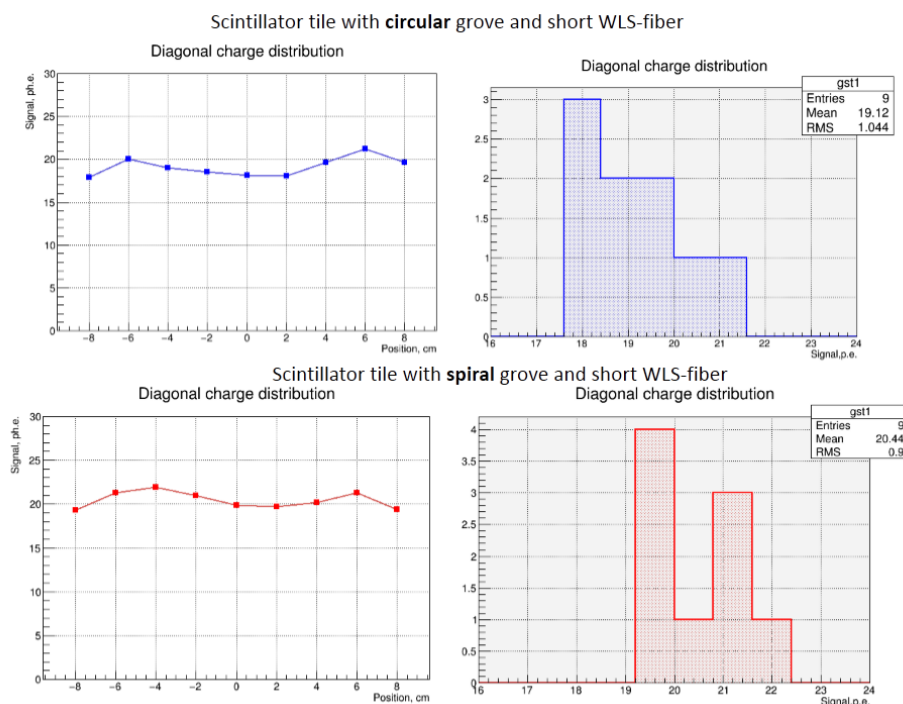
588 To optimize the light collection efficiency from the scintillators some R&Ds on the groove shapes and  
 589 reflectors were performed. Namely, a few types of the scintillator tiles were produced with circular and  
 590 spiral grooves. At present, the most common reflector used in high energy physics for the scintillators  
 591 is the TYVEC film due to its perfect reflection index, stability and cheapness. Nevertheless, the  
 592 preparation of the TYVEC envelopes for each scintillator tile and the wrapping around are rather  
 593 handwork consuming processes. Therefore, other type of reflector was tested which is simply the surface  
 594 treatment of the polystyrene in some chemical solvent. The photos of different scintillator tiles are  
 595 presented in Fig. 41.

596 The tests of all tiles were performed with  $^{90}\text{Sr}$   $\beta$ -source and trigger counter below the scintillator tile to  
 597 detect the electrons passed through the scintillator. The outer end of WLS fiber was glued into special  
 598 optical connector that was viewed by  $1 \times 1 \text{ mm}^2$  Hamamatsu MPPC with the photon detection efficiency  
 599 of about 25%. The measurements of the light amplitude were done with the step of 2 cm along the  
 600 diagonal of the scintillator. Simple estimation gives the electron energy loss in the scintillator of about  
 601 0.8 MeV. First measurement with chemical reflector revealed much worse light yield and uniformity  
 602 comparing to the TYVEC film. Therefore, the shape of the grooves for WLS fibers was optimized with  
 603 TYVEC reflector. Fig. 42 shows the space distribution of the light yield along the diagonals of the  
 604 scintillator tiles with different shapes of the grooves for WLS-fibers. Here the photodetector Hamamatsu  
 605 MPPC with  $10 \mu\text{m}$  cell size was used. One can see, that both, circular and spiral grooves give similar



**Fig. 41:** Photo of scintillator tiles with different reflectors and different shapes of the grooves. Top left - tile with circular groove and chemical treatment of the scintillator surface, top right - tile with circular groove without reflector, down left - tile with spiral groove without reflector, down right - tile with spiral groove and chemical treatment of the scintillator surface.

606 results with the light yield of about 20 photoelectrons and 5% space nonuniformity in the light collection.  
607 The spiral grooves provide slightly better parameters and were selected for the design of FHCAL modules.  
608 These very promising results are obtained due to the advanced light readout scheme. For example, in  
609 some calorimeters in high energy physics the WLS fibers or WLS plates are placed just at the lateral sides  
610 of the scintillators without gluing in the grooves. As a consequence, the resulted space nonuniformity is  
611 a factor of 2 and more worse.



**Fig. 42:** Space distribution of the light yield along the diagonals of the scintillator tiles with different shapes of the grooves for WLS-fibers. The reflector TYVEC is used around scintillator. Top and down panels are for circular and spiral grooves, respectively. Right panels are histograms of the measured light yield expressed in the number of photoelectrons. All the measurements were done with  $^{90}\text{Sr}$   $\beta$ -source and trigger counter below the scintillator tile to detect the electrons passed through the scintillator.

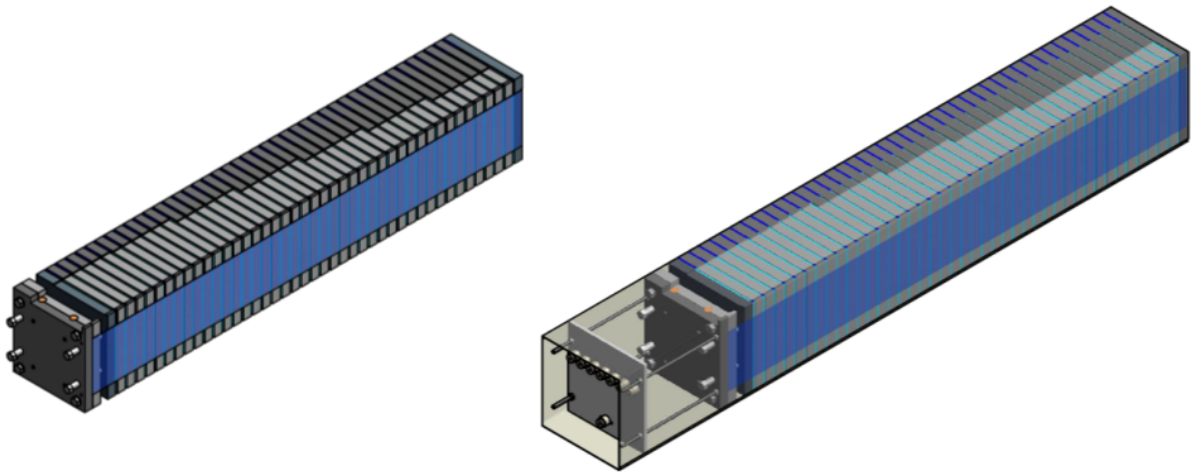
#### 612 4.4 Mechanical design of the modules

613 The mechanical construction of the FHCAL modules should satisfy a few requirements:

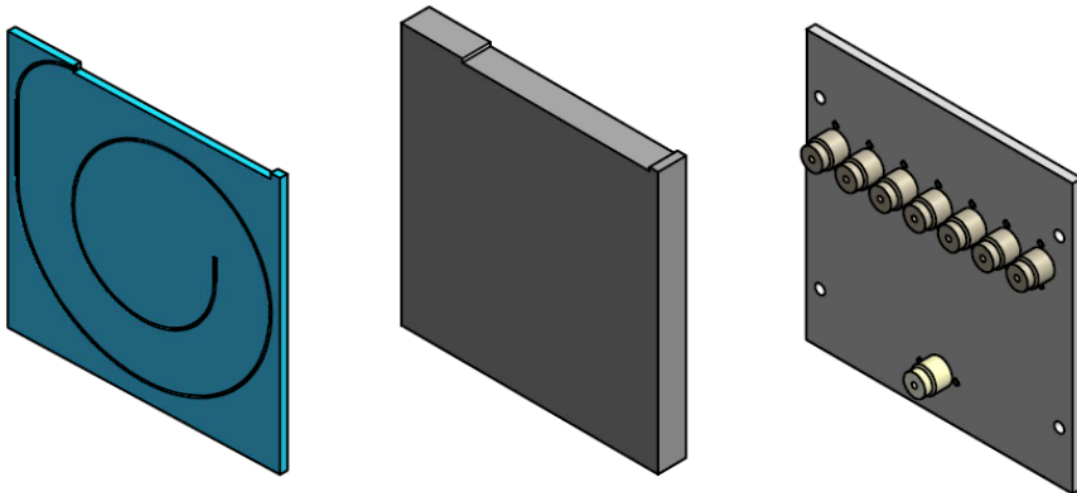
- 614 1. The construction must provide reliable light readout from all 42 scintillator tiles;
- 615 2. It must carry weight of 200 kg;
- 616 3. Each individual module must be transported and installed in the required position;
- 617 4. The dead material between modules must have a minimum thickness to avoid the loss of energy in
- 618 hadron showers.

619 3D-view of the FHCAL module is presented in Fig. 43.

620 All 42 layers of lead/scintillator sandwiches in each module are loaded into box made of 0.5 mm stainless  
 621 sheet and tied together in one block with length about 90 cm (about 4 nuclear interaction lengths) by a  
 622 0.5 mm stainless steel tape. This tape and the box lateral sides are spot-welded together. The WLS-  
 623 fibers from each of 42 scintillator tiles are stretched in 2 mm air gap at the top side of the module. Each  
 624 WLS-fiber is covered by thin black pipe for the light isolation and the mechanical protection. Each 6  
 625 consecutive WLS-fibers from one section are collected in one optical connector at the end of module  
 626 and polished to ensure the optical contact with MAPD. Additionally to 6 WLS-fiber one clear fiber from  
 627 the monitoring system is glued in the same optical connector. Other ends of 7 clear fibers are connected  
 628 together and illuminated by the light emitting diode (LED). Such simple monitoring system provides  
 629 the permanent control for the readout elements. All this structure is covered by another similar stainless



**Fig. 43:** 3d-view of the module without (left) and with the light readout part.



**Fig. 44:** Basic parts of the module. Left - scintillator tile with spiral groove, middle - lead absorber, right - panel with optical connectors.

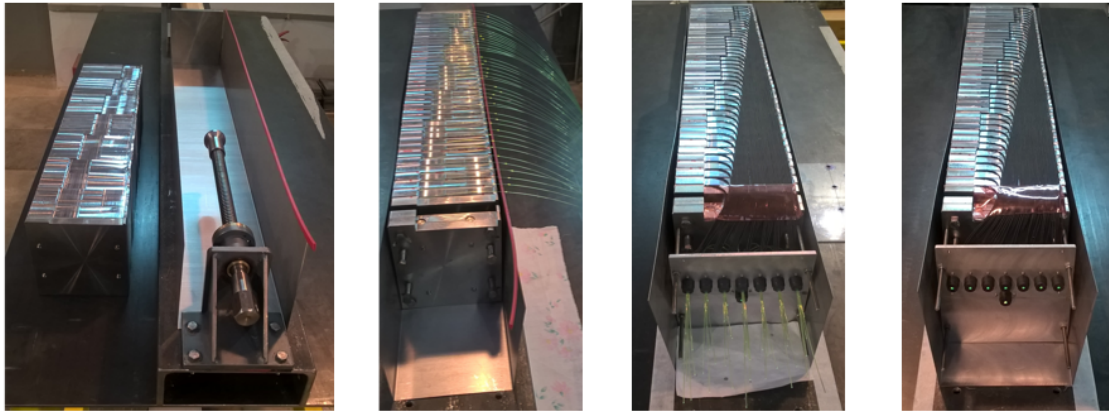
630 box and these two boxes are spot-welded providing the mechanically stable module. The weight of each  
 631 small module with transverse size  $15 \times 15 \text{ cm}^2$  is about 200 kg.

632 Main elements of FHCAL modules are scintillator tiles, lead plates and light readout system, consisting of  
 633 WLS-fibers and the optical connectors at the rear panel of the module. These basic elements are shown  
 634 in Fig. 44. Lead plates have 16 mm thickness and the same shape as scintillator plates. The lead contains  
 635 about 3% of antimony to increase its hardness.

636 Main sequence of the modules assembling is demonstrated in Fig. 45.

637 To confirm the reliability of the FHCAL construction all the components for 9 modules were ordered and  
 638 produced in the middle of 2016. Then 9 modules were assembled and mechanically tested. After the  
 639 tests, all these modules were installed at the frame arranging the  $3 \times 3$  area or supermodule, see Fig. 46.

640 Finally, the light yield of all longitudinal sections was measured by using the cosmic muons crossing all

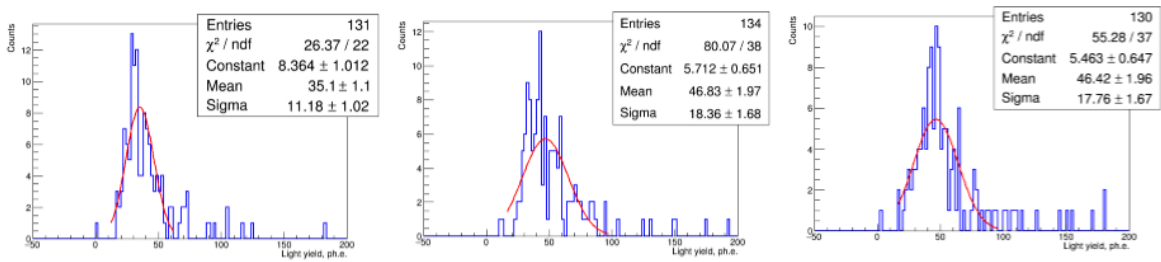


**Fig. 45:** Main stages of module assembling. Left - lead absorbers are ready for the installation into stainless steel box. Center - module with lead/scintillator sandwiches before and after WLS-fiber aligning. Right - each 6 of consecutive WLS fibers and one clear fiber are glued inside the optical connector and polished.



**Fig. 46:** Photo of 9 assembled modules, front view (left) and rear view (right).

641 7 sections in single module. Here the same readout chain (photodetectors, front-end-electronics, readout  
 642 electronics) was used as planned in real calorimeter. The amplitude spectra from minimum ionizing  
 643 particles (MIPs) for a few sections are presented in Fig. 47. As seen, the light yield in one section  
 644 achieves 40-45 photoelectrons for 5 MeV detected energy.



**Fig. 47:** Amplitude spectra in a few longitudinal sections from the horizontal cosmic muons crossed all 7 sections in the module.

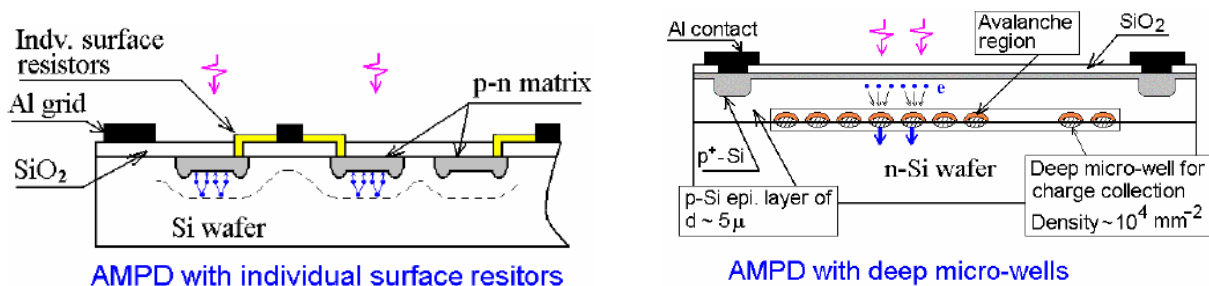
## 645 5 Readout of FHCAL modules

### 646 5.1 Light readout by silicon photomultipliers

647 The principal problem in development of the FHCAL is the choice of the photodetectors for the light  
 648 readout from the WLS-fibers. These photodetectors must be compact enough to set 7 pieces at the rear  
 649 side of the module. Immunity to the solenoid magnetic field and to the nuclear counter effect are also  
 650 key requirements for these readout elements. The avalanche photodiodes, APDs are the natural choice  
 651 in this case. They have been successfully used in electromagnetic calorimeters and have well defined  
 652 and reliable parameters. At the same time, the low (50 – 100) gain of APD requires a sophisticated  
 653 amplifier and limits its capability to detect low intensity light at the level of tens photons. The hadron  
 654 calorimeters have light yield of an ordermagnitude smaller comparing to that for the electromagnetic  
 655 calorimeters. This limitation is essentially critical for the calibration of the calorimeter using minimum  
 656 ionizing particles that produce low energy deposition.

657 Among a few modifications of avalanche photodiodes, the diodes with micropixel structure are of special  
 658 interest because of their remarkable properties [29, 30]. Silicon photomultipliers (SiPM's) or Micropixel  
 659 avalanche photodiodes( MAPD's) are rather novel devices that are intensively developed and applied in  
 660 modern research projects [31–34]. Each pixel in MAPD might be regarded as an individual photodi-  
 661 ode creating an avalanche in limited Geiger mode with the internal gain up to  $\sim 10^6$ . SiPMs have very  
 662 compact dimensions in the scale of a very few millimeters. Due to the pixel structure, MAPD's have  
 663 no nuclear counting effect; they are sensitive to a single photoelectron signal and have remarkable am-  
 664 plitude resolution even for a few photoelectrons signal. The technology of SiPM's production and their  
 665 parameters are sharply improved.

666 As a summary, the main advantages of MAPD's are: very compact sizes, low bias voltage, gain compar-  
 667 able to PMT, relative low price, insensitivity to magnetic field and absence of nuclear counter effect (due  
 668 to the pixel structure). The sketches of two different MAPD types are shown in Fig. 48. The main feature  
 669 of the first type (Fig. 48, left) is that groups of  $p-n$  cells (pixels) are connected to metal electrodes via  
 670 individual surface resistors. Unfortunately, the standard MAPD technology with individual surface re-  
 671 sistors has a strict limit in the number of pixels/mm<sup>2</sup> due to the dead areas around each individual pixel.  
 672 This limitation is prohibitive for the calorimetry applications, in particularly, for the FHCAL. The reason  
 673 is the dynamical range of measured energies. MC simulations described above shows that the detected  
 674 energy in a single section of the FHCAL module reaches 1 GeV . Taking into account the light yield  
 675 up to 10 photoelectrons/MeV, the maximum signal in one section would achieve ten thousands photo-  
 676 electrons. This is true in the case of proportionality between the number of fired pixels (photoelectrons)  
 677 and the number of initial photons. In reality, the limited number of pixels,  $N_{total}$  leads to a nonlinear  
 678 dependence of the number of fired pixels,  $N_{fired}$  on the number of photons,  $N_{photons}$ :



**Fig. 48:** G-APDs with two different structures. Left – SiPM with the individual surface resistors and number of cells (pixels) of about 1000/mm<sup>2</sup>. Right – MAPD with deep micro-wells with the pixel density 15000/mm<sup>2</sup>.

$$N_{fired} = N_{total} \left( 1 - e^{-\frac{N_{photons} PDE}{N_{total}}} \right). \quad (12)$$

679 Using this formula one can estimate the minimum number of pixels required for measured energy range.  
 680 For the case of  $3 \times 3 \text{ mm}^2$  MAPD, the pixel density must be up to  $10000/\text{mm}^2$  to ensure a linear MAPD  
 681 response. Ordinary SiPM's with surface resistors have pixel density  $\sim 1000/\text{mm}^2$  that is certainly not  
 682 sufficient.

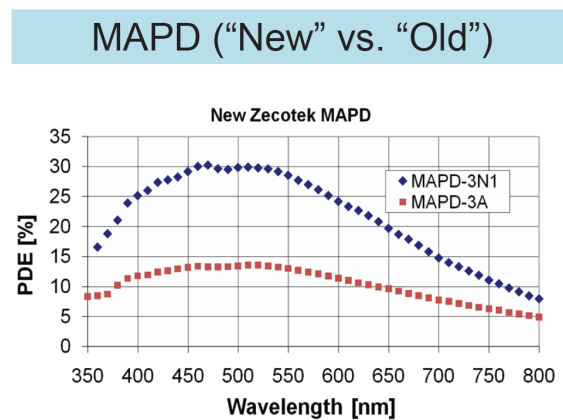
683 At present, another advanced technology of MAPD production exists based on the creation of pixels  
 684 with the use of electric field distribution inside the silicon wafer (Fig. 48, right). Produced in such a  
 685 way MAPDs have a pixel density about  $10000 - 20000/\text{mm}^2$ . These MAPDs were initially produced  
 686 by JINR (Dubna, Russia) in collaboration with the Mikron Company (Zelenograd, Russia). At present,  
 687 this technology is successfully applied by Zecotek Co. ([www.zecotek.com](http://www.zecotek.com)). There are a few R&D  
 688 projects [35, 36], where similar MAPDs are successfully used.

689 Last few years a nice success in the development of the SiPM's with high dynamic range was achieved  
 690 by Hamamatsu Co. (Japan) that produces a few types of photodetectors with the pixel (or cell) density up  
 691 to  $10000/\text{mm}^2$ . Moreover, the recovery time of the pixels with the size  $10 \times 10 \mu\text{m}^2$  achieves impressive  
 692 10 ns. Taking into account the length of the light pulse from WLS fiber as 50 ns, the equivalent number  
 693 of pixels would be about  $30000/\text{mm}^2$ .

## 694 5.2 Properties of selected photodiodes

695 As mentioned above the FHCAL readout requires special types of Silicon photomultipliers (SiPM's)  
 696 or Micropixel avalanche photodiodes (MAPD's) with very high pixel density to ensure an appropriate  
 697 dynamic range of the detected energies in the calorimeter. At present there are a few types of the pho-  
 698 todiodes that satisfy this requirement. Two types of the photodetectors are produced by the by Zecotek  
 699 Co. These are so called MAPD-3A and MAPD-3N types with the pixel density  $15000/\text{mm}^2$ . They have  
 700 a photon detection efficiency (PDE) of about  $15 - 30\%$  at  $500 - 550 \text{ nm}$  (Fig. 49) that is well matched  
 701 with the emission spectrum of WLS-fibers. The PDE is the product of three values: quantum efficiency  
 702 which is about  $70 - 90\%$  for normal APDs; geometrical factor, that reflects the fraction of the active area  
 703 respective whole APD square and probability to initiate the Geiger discharge.

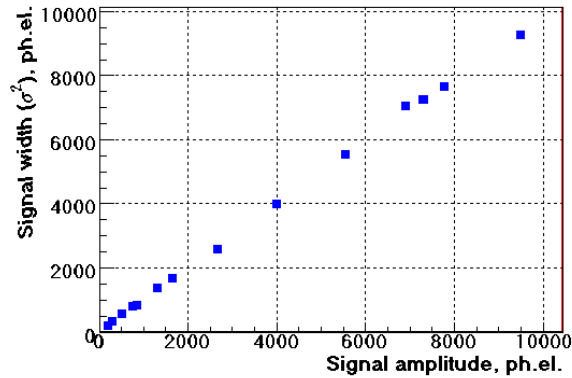
704 The working voltage ranges from  $60 \text{ V}$  to  $90 \text{ V}$  depending on the type of MAPD. The gain of these  
 705 MAPDs is about  $5 \times 10^4$  and additional amplifier with amplification a factor a few tens is needed.



**Fig. 49:** The PDE of MAPD (Zecotek) with pixel density  $10^4/\text{mm}^2$  and active area  $3 \times 3 \text{ mm}^2$  as a function of light wavelength.

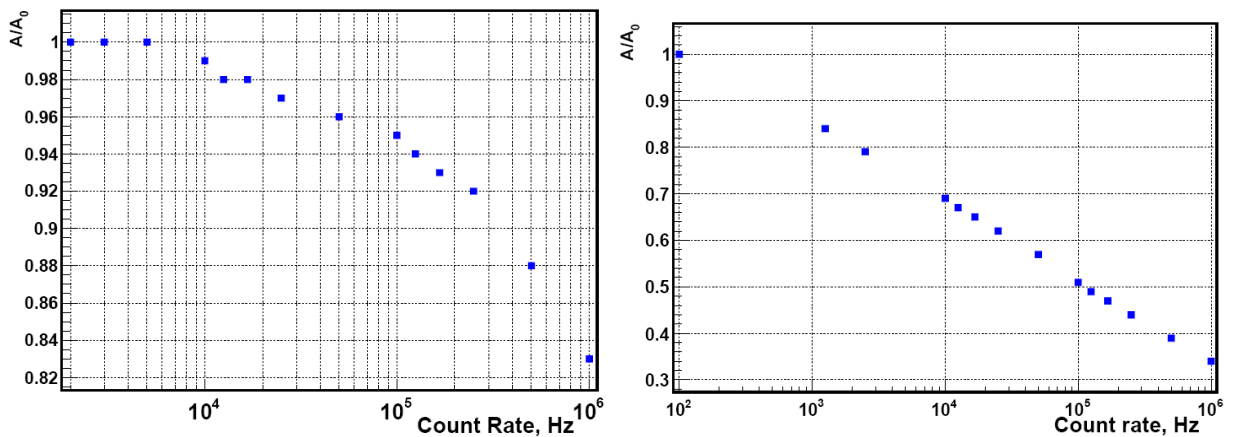


706 The huge pixel density ensures linearity of the signal response up to 15000 photoelectrons that is rather  
 707 safe for NICA energies. Linearity was measured by illuminating the selected  $3 \times 3 \text{ mm}^2$  MAPD by the  
 708 light emitting diode with variable light intensity. In case of linear response the square of the signal width  
 709 (square of sigma) must be equal to the signal amplitude if both parameters are measured in number of  
 710 photoelectrons. As seen in Fig. 50, the linearity is preserved up to  $10^4$  photons that it sufficient for the  
 711 detected energies in FHCAL at MPD/NICA experiment.



**Fig. 50:** The dependence of the signal width for  $3 \times 3 \text{ mm}^2$  MAPD irradiated by LED on the signal amplitude. Here  $Y$ -axis is the square of sigma of the signal distribution expressed in the number of the photoelectrons.

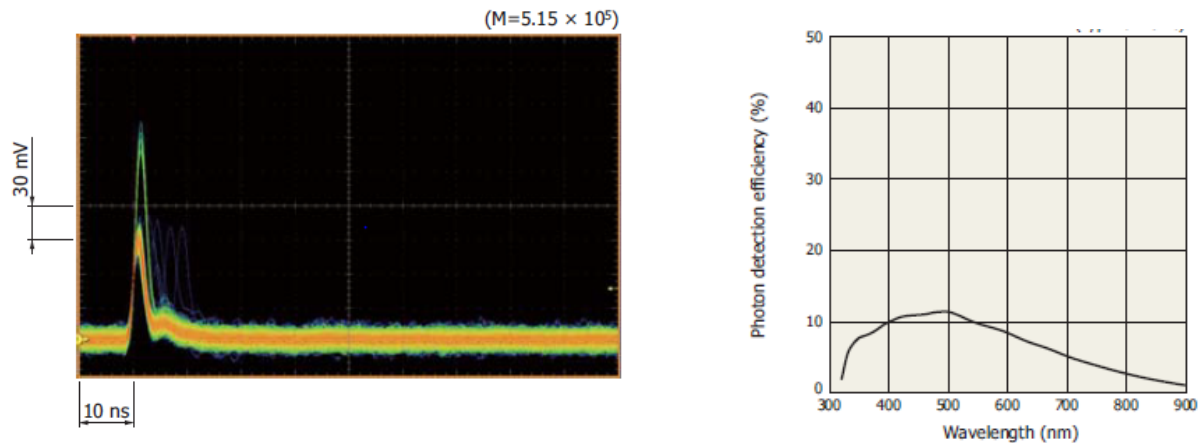
712 According to Fig 49 the MAPD-3N type is more attractive because of its higher PDE value. At the  
 713 same time, there is a the problem with the recovery time of individual pixels in MAPD. Therefore,  
 714 measurements of the amplitude variation depending on the illuminating LED signal frequency were  
 715 performed. Fig. 51 presents the relative photodiode amplitude behavior for both MAPD-3A and MAPD-  
 716 3N types. It is obvious that MAPD-3N amplitude is extremely sensitive to the count rate that cannot be  
 717 accepted. At the same time, MAPD-3A could work at a counting rate of about  $10^4$  Hz without significant  
 718 amplitude reduction. As seen from the plot, at a frequency  $10^4$  Hz and average light signal of about 1500  
 719 photoelectrons the drop of MAPD amplitude is about 1%. Therefore, MAPD-3A is a good candidate as  
 720 FHCAL photodetector.



**Fig. 51:** Relative change of MAPD amplitude with the frequency of LED signal. Initial MAPD amplitude is about 1500 photoelectrons that correspond to  $\sim 200 \text{ MeV}$  of visible deposited energy. Left – MAPD-3A, right – MAPD-3N.

721 Quite recently Hamamatsu Co. offered another type of silicon photomultiplier, so called multipixel pho-

722 ton counter (MPPC) with extremely small pixel size  $10 \times 10 \mu\text{m}^2$ , type S12572-010C/P. It corresponds  
 723 to a pixel density of  $10000/\text{mm}^2$  that is factor of 1.5 less than in MAPD-3A. But the pixel recovery time  
 724 and the signal width of S12572-010C/P type (Fig. 52, left) is less than 10 ns. These extremely fast pixels  
 725 can be recovered a few times during 50 – 60 ns light signal from WLS-fibers. It means that the equiva-  
 726 lent density of the pixels in S12572-010C/P type is a few times larger than that of MAPD-3A providing  
 727 excellent dynamic range. Note, that other parameters of these MPPC (gain and PDE) are rather similar  
 728 to that in MAPD-3A type, see Fig. 52, right.



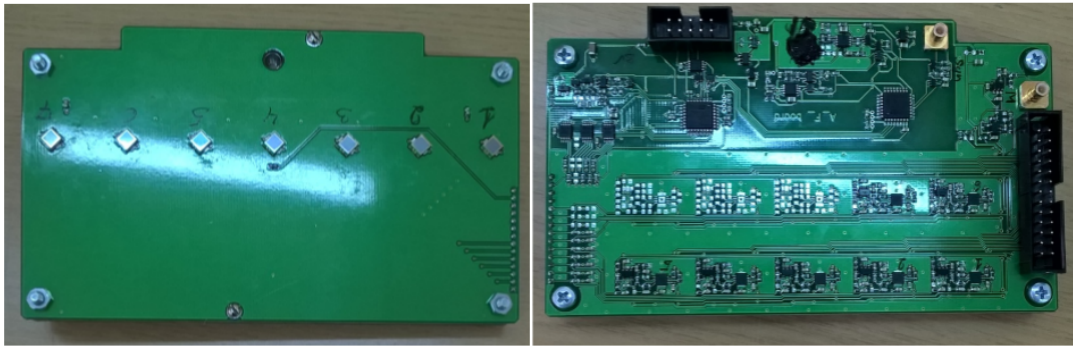
**Fig. 52:** Left – the shape of single electron pulses of MPPC S12572-010C/P with high pixel density. Right – the dependence of photon detection efficiency of MPPC on the wavelength.

729 In summary one can conclude that at least two types of photodetectors satisfy the FHCAL requirements  
 730 and can be used there as photodetectors.

### 731 5.3 Front-end and readout electronics

732 The Front-End-Electronics (FEE) must satisfy to the parameters of the input signals after the photodetec-  
 733 tors and to the dynamic range of the detected energies. Since the SiPMs (MAPDs) have a gain of about  
 734  $5 \times 10^4$ , the readout electronics needs additional amplification factor of 10. The lowest detected energy is  
 735 deposited by the minimum ionizing particles (MIP) that will be used for the FHCAL calibration. In this  
 736 case the energy deposition in the scintillator plates in one section is about  $5 \text{ MeV}$ . The maximum energy  
 737 deposition would be in case of fragments hits of inner FHCAL modules around the beam axis. Since  
 738 the visible energy deposited in the scintillator is only about 2.5% of full energy deposited in FHCAL  
 739 modules, it would achieve one  $\text{GeV}$ . It means that the dynamic range of detected energies could achieve  
 740 factor of 200 at maximum. To fulfill this requirement we developed FEE with one stage amplification of  
 741 the input signal. The photos of developed FEE for the FHCAL module prototype are shown in Fig. 53.  
 742 FEE is deployed at two PCBs. The photodiodes are placed at first PCB, while the second PCB serves for  
 743 amplifiers, the individual voltage sources for each MAPD and also for the Light-Emitting-Diode (LED)  
 744 source of calibrated light pulses used for the monitoring of the MAPD gains. Signals after amplification  
 745 have separate outputs in IDC connector. Since the FHCAL module has 7 longitudinal sections, FEE has  
 746 7 MPPCs and 7 output analog signals.

747 FEE additionally has an analog adder that sums up the signals from all 7 sections. This adder signal is  
 748 used for the arrangement of the trigger signal from a single module.



**Fig. 53:** The photos of FEE developed for the FHCAL module. It consists of 2 PCB boards. The photodiodes are placed at first PCB, while the second PCB serves for amplifiers and the individual voltage sources for each SiPM.

749 As the readout electronics of FHCAL the ADC64s2 board is used. ADC64s2 (see Fig. 54) is a 64-channel  
 750 12-bit 62.5 MS/s ADC device with signal processing core and Ethernet interface. It has dedicated serial  
 751 links for clock synchronization and data readout that allows system scalability to arbitrary number of  
 752 channels. ADC board is a waveform digitizer of the analogue input signal and samples it at fixed time  
 753 intervals. Zero suppression logic is based on baseline estimation and threshold value. It allows to reduce  
 754 the number of waveform points required for digital signal representation with minimum loss of accuracy.  
 755 The ring type memory allows the read back of last 30  $\mu$ s of waveforms. ADC board might be integrated  
 756 to the White Rabbit precise synchronization system for large distributed systems. This system is also  
 757 intended for the deterministic and reliable data delivery.



**Fig. 54:** The photo of ADC64s2 board planned for the FHCAL readout.

## 758 **6 Beam test results of the FHCAL module prototypes**

759 To study the reliability of the proposed concept and the technical design of the lead/scintillator sand-  
760 wich calorimeter a few R&Ds have been performed during the last years. Also the parameters of the  
761 calorimeter prototypes were studied in a few beam tests.

762 In frames of these R&Ds a few small modules with the transverse size  $10 \times 10 \text{ cm}^2$  and large modules  
763 with the transverse size  $20 \times 20 \text{ cm}^2$  have been constructed. Detailed study of the calorimeter modules  
764 response in the hadron energy range from a few  $\text{GeV}$  up to  $160 \text{ GeV}$  has been performed. Quite recently  
765 a few prototypes of FHCAL modules were assembled and tested with the cosmic muons.

766 Since the transverse profile of the hadron shower is comparable with the interaction length ( $17.1 \text{ cm}$   
767 for the lead), the calorimeter must have appropriate transverse sizes to minimize the lateral leakage of  
768 hadronic shower. Also, to study the rear shower leakage the length of the calorimeter must be long  
769 enough. For these reason one FHCAL large module with the transverse sizes  $20 \times 20 \text{ cm}^2$  and the length  
770 of about  $6\lambda_i$  has been constructed and used for the beam tests in energy range of  $2 - 6 \text{ GeV}$  at CERN.  
771 This module has 10 longitudinal sections instead of 7 ones in real FHCAL desing. The weight of large  
772 prototype is about  $500 \text{ kg}$ , i.e. 2.5 times heavier of the real FHCAL module.

### 773 **6.1 Test of FHCAL module prototype at low proton energies**

774 The FHCAL at MPD/NICA will work at low beam energies of about  $2-6 \text{ GeV}$ . In this region the response  
775 of the calorimeter is different for pions and protons due to the limited hadron shower development for  
776 proton energies below  $5 \text{ GeV}$ . This feature requires an additional experimental study at low proton  
777 energies. For this purpose, the large FHCAL module prototype with transverse size  $20 \times 20 \text{ cm}^2$  has been  
778 tested at T10 PS beam line, CERN (Fig. 55). This beam line provides the hadrons with the momentum  
779  $2 - 6 \text{ GeV}/c$ .



**Fig. 55:** Layout of large module at T10 PS beam line, CERN.

780 Time of flight (TOF) method was used to separate the protons from pions in the secondary beam at T10  
781 beam line. Two Cherenkov detectors with transverse sizes  $20 \times 20 \text{ mm}^2$  measured the TOF of beam  
782 particles. One of these detectors was installed at the center of the front surface of large module (Fig. 55,  
783 right) and another one was placed at a distance of about 15 meters upstream.

784 Two-dimensional ADC-TOF spectra for two incident momenta of particles –  $2$  and  $6 \text{ GeV}/c$  are shown  
785 in Fig. 56. The time resolution of the Cherenkov detector was about  $50 \text{ psec}$ . Good separation of pions  
786 and protons was observed in full momentum range of  $2 - 6 \text{ GeV}/c$ .

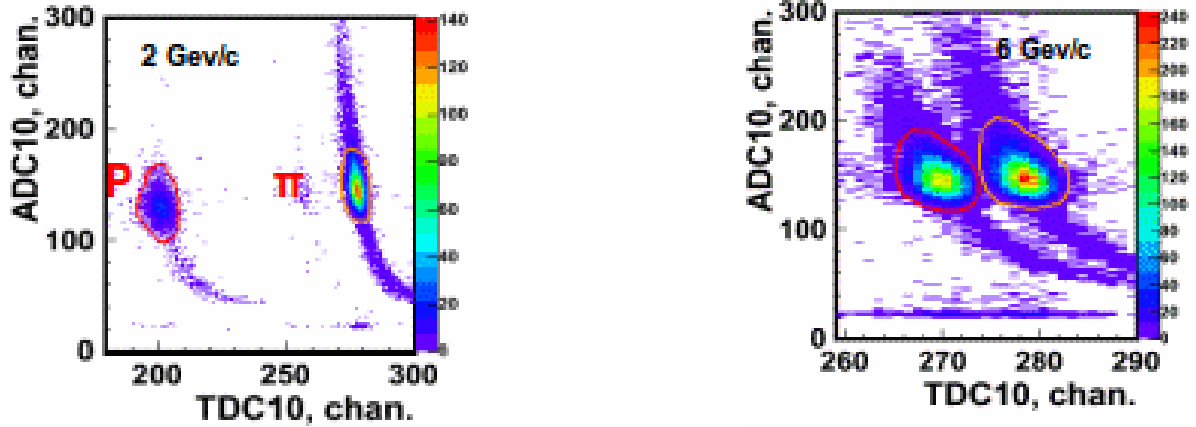


Fig. 56: Two dimensional ADC-TOF plots for 2 GeV/c beam particles (left) and 6 GeV/c particles (right).

787 Muons in T10 beam line have been used for the calibration of the calorimeter module. Spectra of energy  
 788 depositions from muons in each of 10 sections are shown in Fig. 57. Good separation of muon peaks from  
 789 the pedestals was observed. As seen in Fig. 57, the pedestal (left) peaks in ADC spectra have different  
 790 heights, because the muons after beam stopper have wide energy spectrum and are absorbed in different  
 791 sections depending on the initial energy. Nice amplitude spectra from the minimum ionizing particles  
 792 provide a powerful tool for the energy calibration of FHCAL module in real experimental conditions as  
 793 would be discussed further.

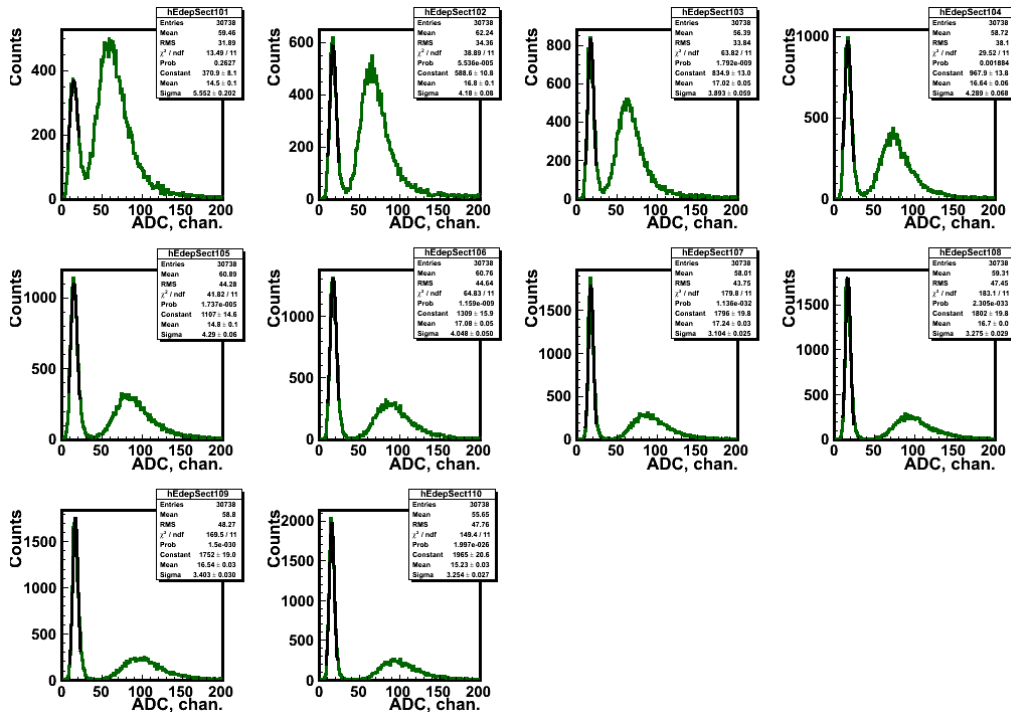


Fig. 57: Amplitude spectra of muon energy depositions in each of the 10 sections of the module. Left peaks correspond to pedestals of ADC.

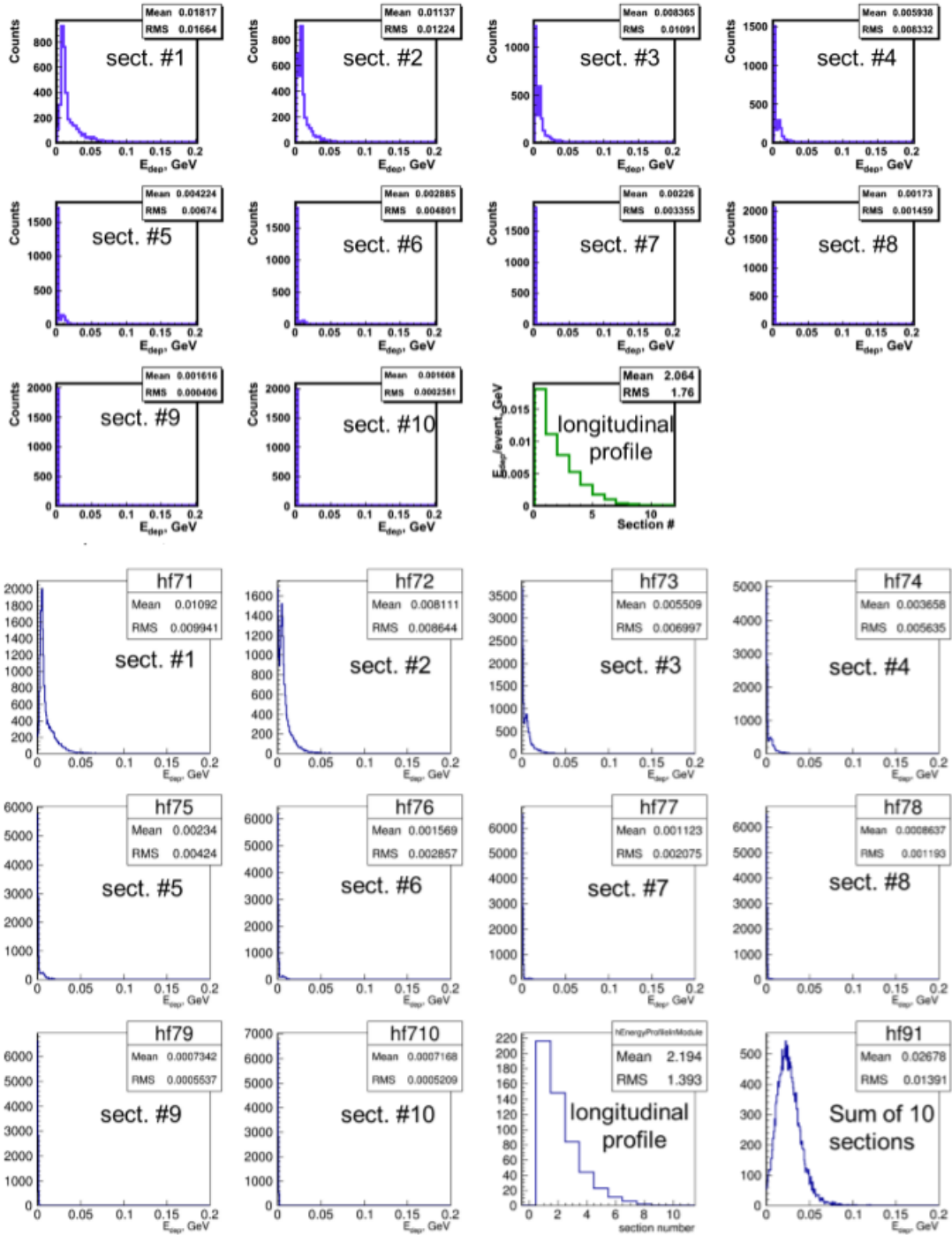
## 794 **6.2 Response of FHCAL module prototype to low energies**

795 To study the hadron shower profile from protons with low energies the amplitude spectra in each of  
796 10 sections were plotted for the beam momenta in the range  $2\text{ GeV}/c - 6\text{ GeV}/c$ . The experimentally  
797 measured energy depositions from  $2\text{ GeV}/c$  and  $6\text{ GeV}/c$  protons in each of 10 sections of the module  
798 are presented in Fig. 58 and 59, respectively. Also the results of GEANT4 MC simulations are shown  
799 there for the comparison. One can see very good agreement between experiment and MC simulation  
800 in the shapes of energy spectra in the individual sections and in the longitudinal profiles of the hadron  
801 showers. The maximum of the hadron shower corresponds to the first half of the interaction length (first  
802 section), where about 20%-30% of full hadron energy is deposited. First section is especially prominent  
803 for the lowest  $2\text{ GeV}/c$  proton momentum. Also at this momentum the energy deposition components  
804 from the ionization loss and hadronic shower are not visually separated. For higher momenta  $3\text{ GeV}/c$   
805 and  $4\text{ GeV}/c$  these two components in energy deposition are clearly seen, see Fig. 60.

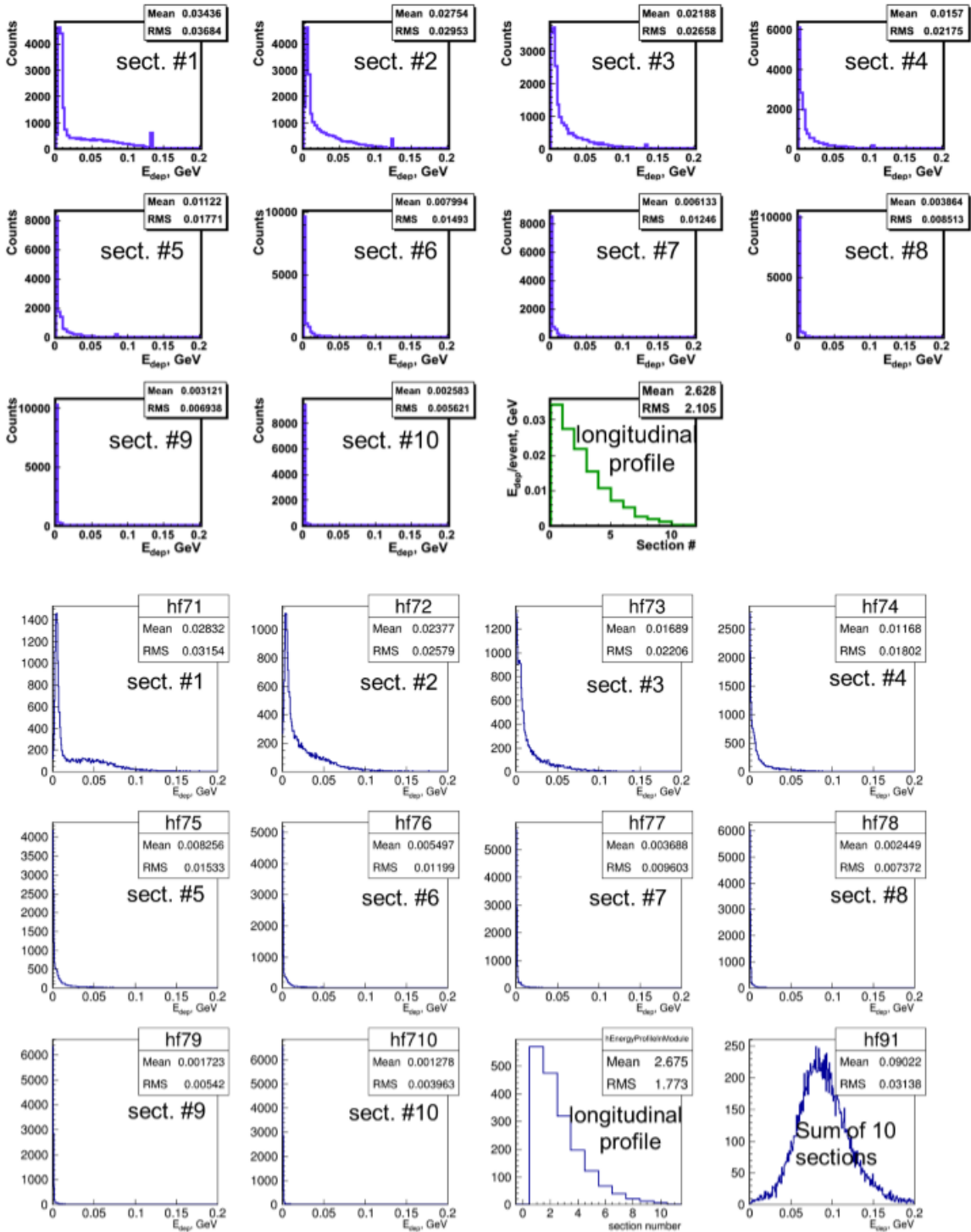
806 The importance of the first section is significant for the detection of the electromagnetic particles too,  
807 because practically full photon/electron energies are deposited there. Maximum fraction of the hadron  
808 energy in first section reveals a serious problem in the separation of the hadron and electromagnetic  
809 contributions in the energy depositions that would be discussed below.

810 Note, that the energy depositions from pions at low energies are quite different. As seen in Fig. 61,  
811 the contribution from the hadronic shower is well observed even for the minimum pion momentum of  
812  $2\text{ GeV}/c$ . Here ten distributions of proton deposited energies are shown for 10 cases – energy deposition  
813 in first section, sum of energy depositions in two first sections etc. up to sum of energy depositions in  
814 all 10 sections. Similar distributions at different beam energies are used for the estimation of the energy  
815 resolutions of the module with different number of the longitudinal sections.

816 The most important observation in the hadron shower profiles is that the length of FHCAL module proto-  
817 type of 10 sections is excessive to detect low energy protons. The module length might be shortened to  
818 7 sections. Only a small rear shower leak of a few percent exists for the highest proton momenta. This is  
819 an experimental confirmation that the FHCAL modules for MPD/NICA experiment might have 7 sections  
820 to fit the available space inside the magnet.

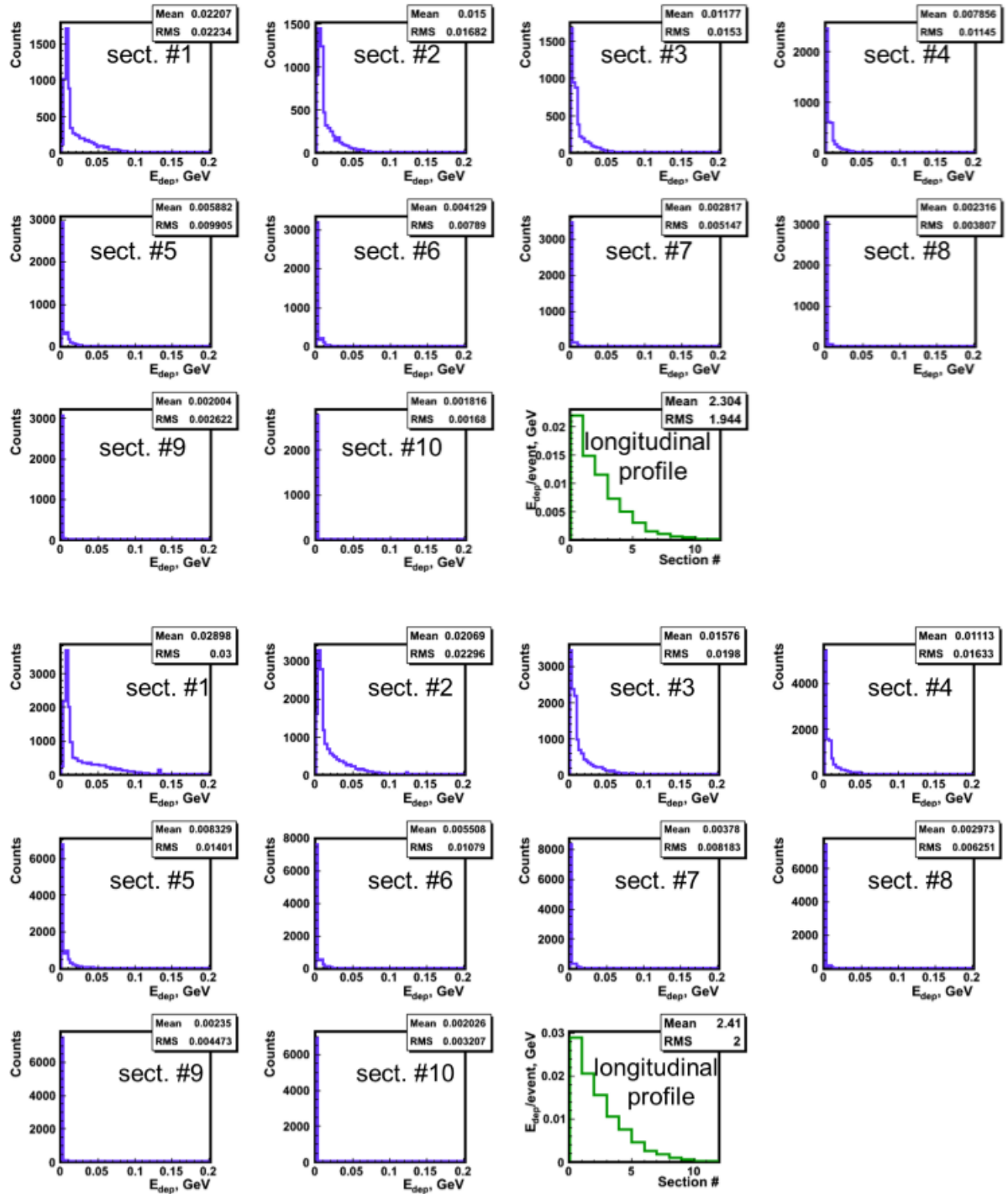


**Fig. 58:** Energy depositions in the sections and the longitudinal profile of hadron shower of calorimeter from incident protons with momenta  $2\text{ GeV}/c$ , experimental data(top panels) and simulated data (down panels).

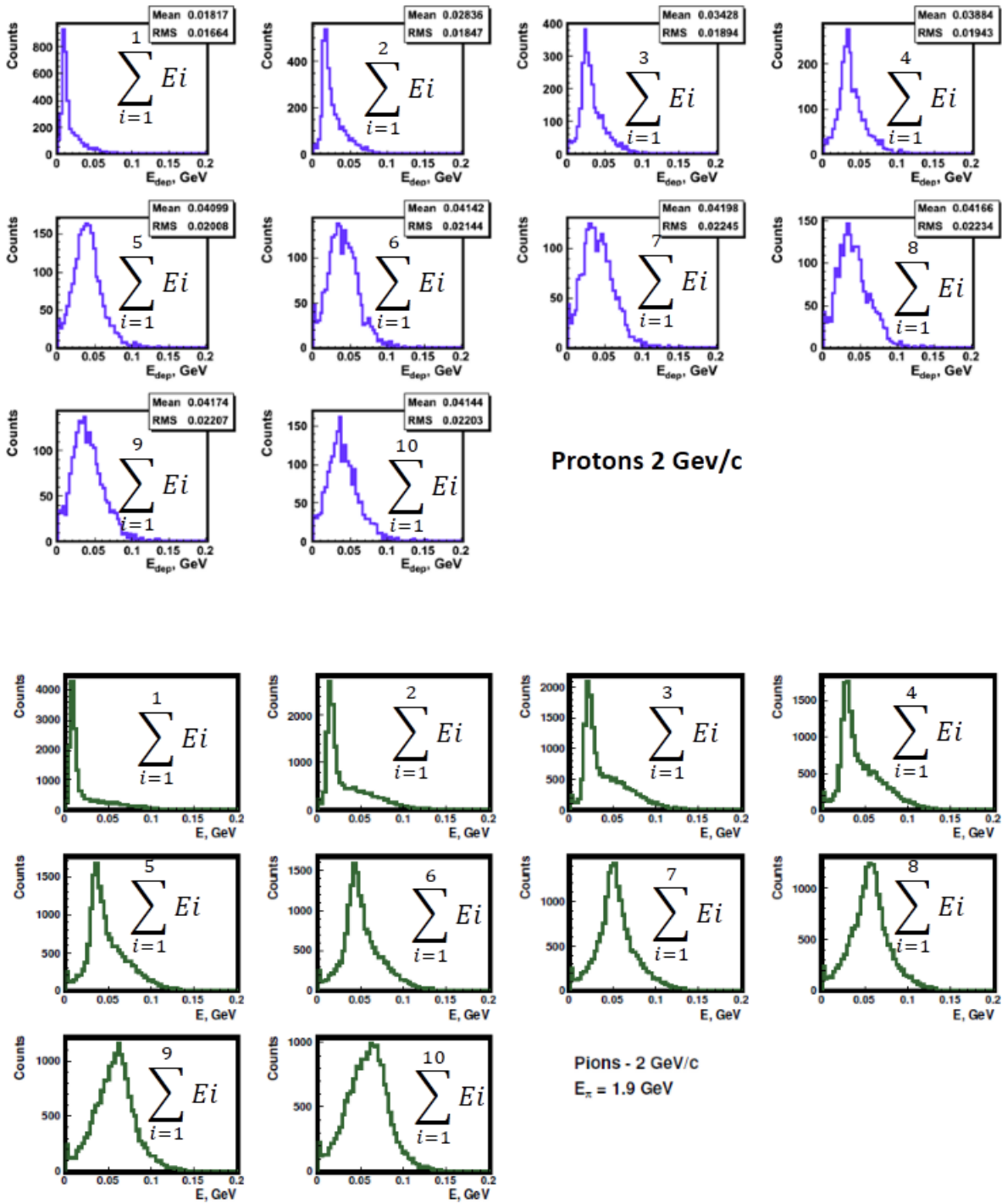


**Fig. 59:** Energy depositions in the sections and the longitudinal profile of hadron shower of calorimeter from incident protons with momenta  $6 \text{ GeV}/c$ , experimental data (top panels) and simulated data (down panels).





**Fig. 60:** Experimental energy depositions in the sections and the longitudinal profile of hadron shower of calorimeter from incident protons with momenta  $3 \text{ GeV}/c$  (top panels) and  $4 \text{ GeV}/c$  (down panels).



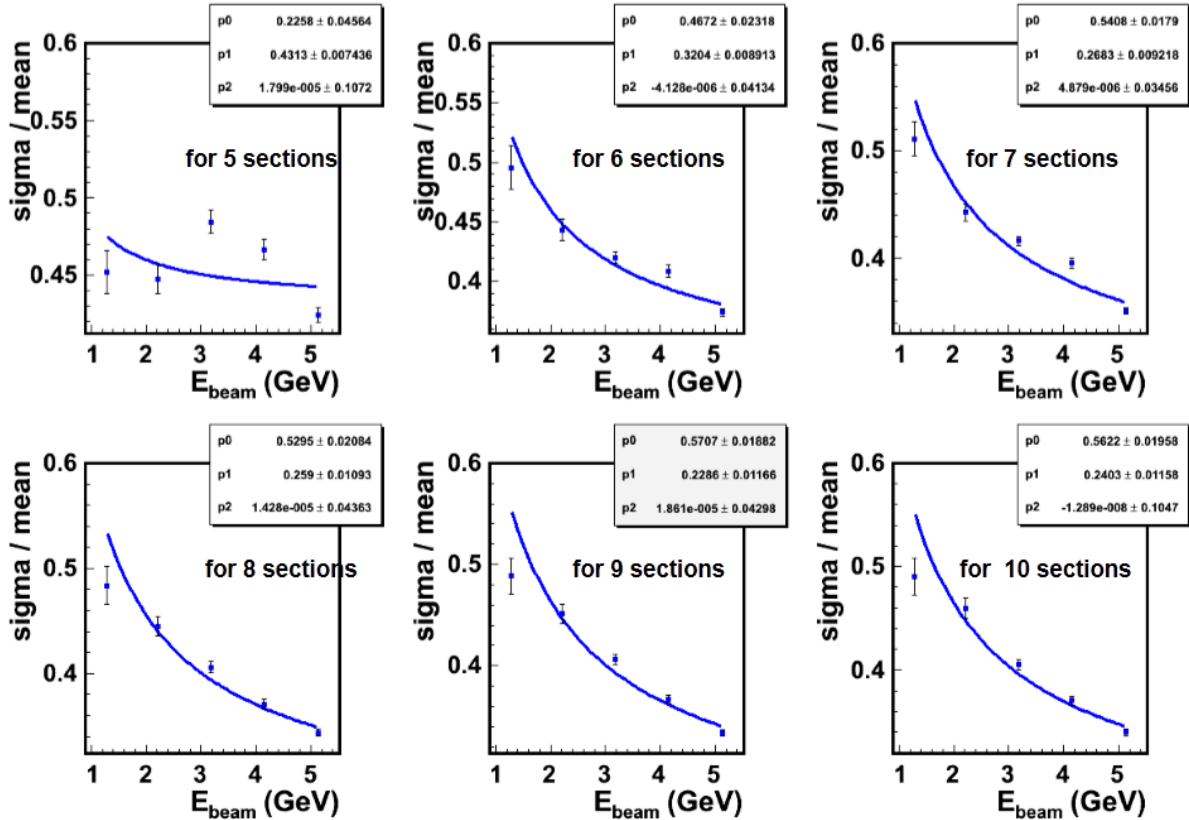
**Fig. 61:** Sum of energy depositions in the sections of calorimeter from incident protons with momenta 2 GeV/c (top) and from incident pions with momenta 2 GeV/c (down). Here ten distributions of deposited energies are shown for 10 cases – energy deposition in first section, sum of energy depositions in two first sections etc. up to sum of energy depositions in all 10 sections.

### 6.3 Energy resolution of FHCAL module prototype at low energies

The plotted above distributions of the energy depositions in sections of the FHCAL module prototype allow the determination of the energy resolution at the different proton energies and for different module configurations. Fig. 62 presents the dependence of energy resolution of the FHCAL module prototype on the kinetic energy of proton beam for different number of used longitudinal sections. The standard parameterization of the energy resolution with three terms is applied:

$$\frac{\sigma_E}{E} = \frac{a}{\sqrt{E}} \oplus b \oplus \frac{c}{E}. \quad (13)$$

Here  $a$  ( $p0$ ),  $b$  ( $p1$ ) and  $c$  ( $p2$ ) are stochastic, constant and noise terms, respectively.



**Fig. 62:** Dependence of energy resolution of the FHCAL module prototype on the kinetic energy of proton beam for different module configurations (number of sections used).

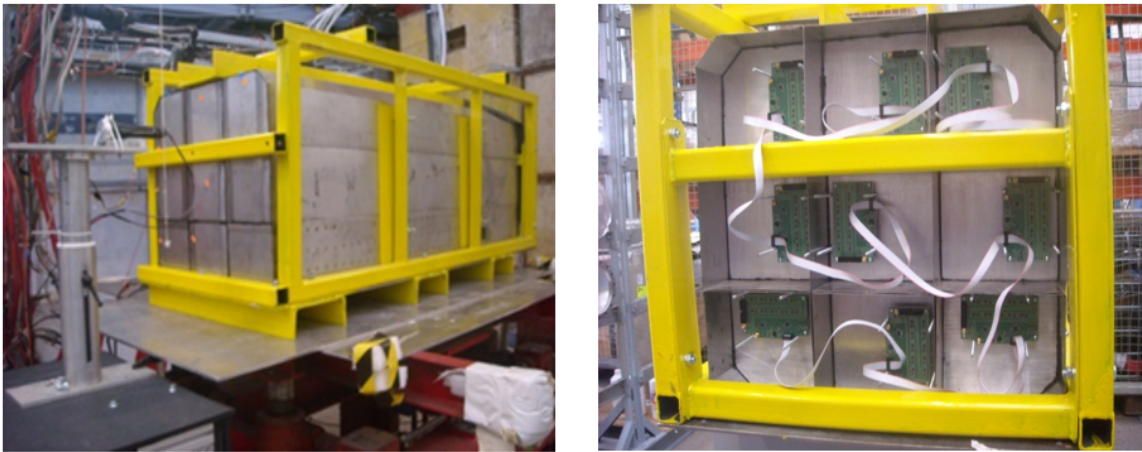
As seen, the energy resolution at the proton energy of 1.2 GeV is about 50% even for half-length module of 5 sections. For the highest kinetic energy of 5.2 GeV the energy resolution is about 35% and practically constant for module length of 7 – 10 sections. It again confirms that the modules length for MPD/NICA experiment might be chosen equal to 7 sections. Unfortunately, short range of measured energy and lateral leak of the shower don't allow the reliable fit of the experimental points with the standard energy resolution function with three (stochastic, constant and noise) parameters. It will be done later for larger calorimeter prototype and wide range of beam energies.

Note, that the measurements at low energies were performed with the MAPD-3N photodiodes that have the described above problem with the count rate capability. Therefore, the energy resolution might be

837 degraded at high count rate, especially at larger beam momenta, where the trigger rate could achieve 1  
838 kHz.

#### 839 **6.4 Study of the FHCAL supermodule response at low energies**

840 The above beam tests were performed with a single FHCAL module. Certainly, the obtained energy res-  
841 olution is degraded due to the lateral leak of the hadron shower. Additionally, the used photodetectors  
842 (MAPD-3N photodiodes) were too slow and also affect the resolution. Another serious drawback of pre-  
843 vious tests is that Front-End-Electronics was not dedicated for the FHCAL. To avoid all these drawbacks  
844 an additional beam test of FHCAL supermodule was performed in the end of 2017. For these purpose a  
845 new  $3 \times 3$  array (supermodule) of FHCAL modules has been constructed. Here we used larger size mod-  
846 ules with 10 longitudinal sections. This feature helped much to understand the optimum length of the  
847 modules for MPD experiment. All 9 small modules with transverse size  $20 \times 20 \text{ cm}^2$  were constructed  
848 at INR (Moscow) and assembled in  $3 \times 3$  array (Fig. 63) to transport it to CERN.



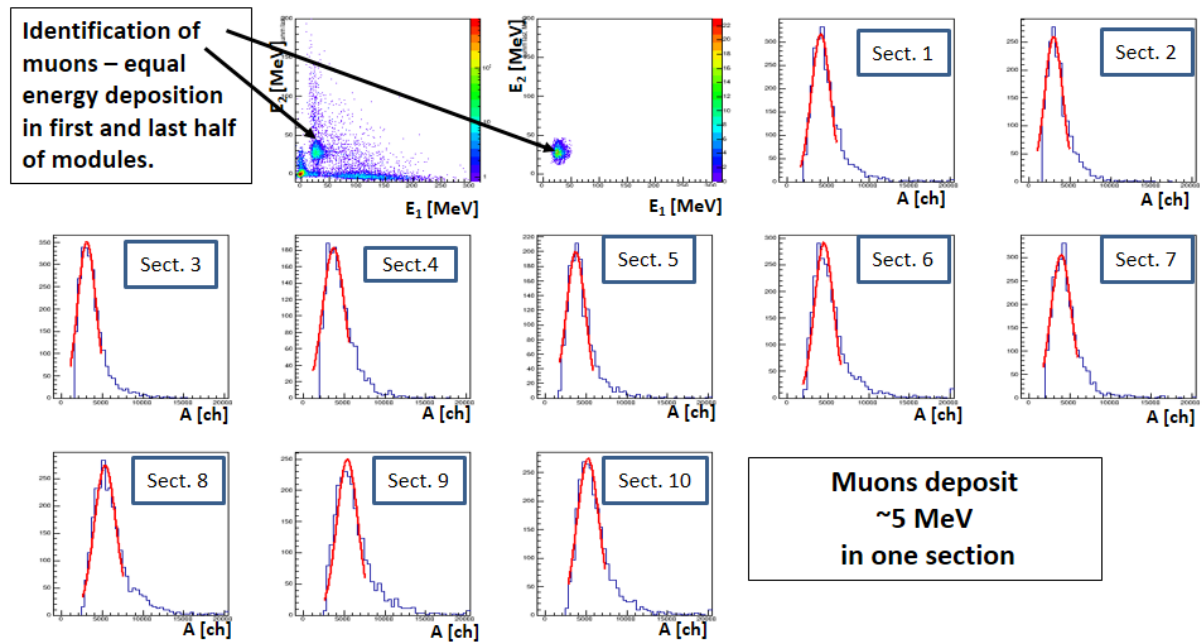
**Fig. 63:** Fully assembled supermodule: front view (left) and rear view (right). The Front-End-Electronics is attached to the optical connectors at the rear side of the modules.

849 The supermodule was installed on a platform at the T9 PS beam line. The readout of all modules was pro-  
850 vided by silicon photomultipliers Hamamatsu MPPC. The attached Front-End-Electronics was specially  
851 developed for MPD experiment that makes possible to study the electronic noise in realistic conditions.

852 The T9 PS beam line has a momentum range for protons and pions from 2 GeV/c to 10 GeV/c that  
853 nicely overlapped the range of the NICA beam energies. Identification of the protons was done by  
854 the gas Cherenkov counter installed upstream of the T9 beam line. The efficiency of the pion/proton  
855 discrimination is degraded at low momentum. Therefore, the data at 2 GeV/c were not analyzed. Also,  
856 there might be some pion contamination in the proton data at 3 GeV/c momentum. Two scintillator beam  
857 defining counter were installed in front of supermodule to identify the beam direction.

858 In the same way, as discussed above, the energy calibration was done using the amplitude spectra of  
859 muon energy depositions in the longitudinal sections of the modules. Note, that the muon spot at the  
860 face of supermodule was wide enough to calibrate all 9 modules without the movement of the platform.  
861 Only the beam defining counters were moved from one module to another one to get the muon data for  
862 all 9 modules. To identify the muons the two-dimensional correlation between energy depositions in first  
863 and last half of the module was plotted. The muons must correspond to the events with the same energy  
864 deposition in all 10 sections as seen in Fig. 64. Here the 6 GeV/c beam momentum was used.

865 After the identification of the muons the amplitude spectra of selected events were plotted and fitted by



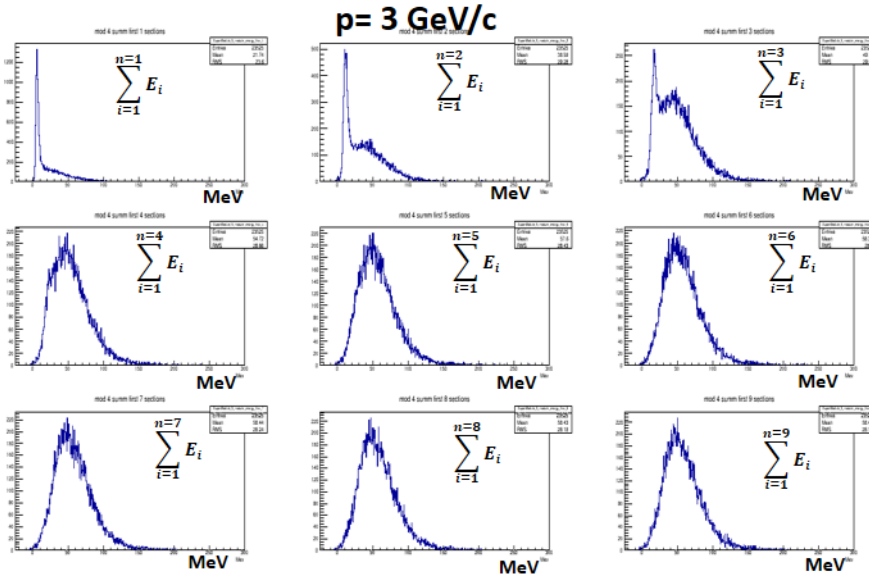
**Fig. 64:** The principle of the identification of the muons and the amplitude spectra used for the energy calibration of FHCAL modules with muon beam.

866 Gaussian. The calibration coefficients we evaluated taking into account that the muon energy deposition  
 867 in each longitudinal section is about 5 MeV. Then the central module of the calorimeter was irradiated by  
 868 proton beam with 5 momenta from 3 GeV/c to 10 GeV/c. During the analysis the amplitude spectra in  
 869 each section were analyzed. For example, Fig. 65 and Fig. 66 show the energy deposition spectra for the  
 870 beam momenta 3 GeV/c and 6 GeV/c, respectively. Here nine distributions of proton deposited energies  
 871 are shown for 9 cases – energy deposition in first section, sum of energy depositions in two first sections  
 872 etc. up to sum of energy depositions in 9 sections.

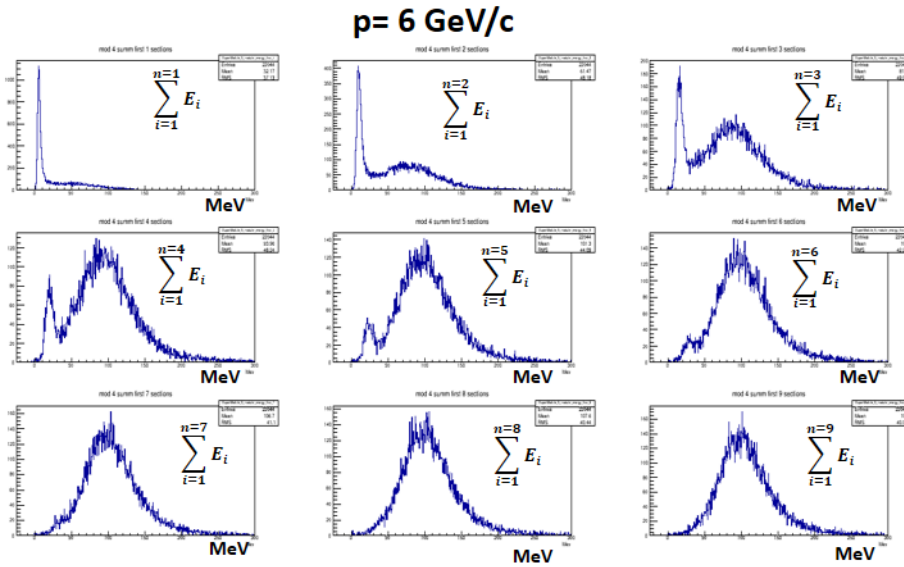
873 One can clearly see two components of the proton energy depositions. The sharp peak in a few first  
 874 sections corresponds to the ionizing energy losses, while long tail is related to the nuclear proton interac-  
 875 tion with the subsequent hadron shower development. For 3 GeV/c proton momenta the ionizing energy  
 876 peak is observed in first 3 sections. The most important observation is that shape of the energy spectra  
 877 is Gaussian-like for 7-th section in both cases. Note, that 6 GeV/c proton momentum corresponds to the  
 878 maximum beam energy of NICA facility. In means, that FHCAL will have normal energy spectra even  
 879 with rather short module length of 7 longitudinal sections.

880 To cross-check the agreement of experimental and simulated data Fig.67 shows the energy spectra in  
 881 first four sections for the 3 GeV/c proton momentum. A good agreement for both types of spectra is  
 882 observed.

883 The energy resolution is the basic parameter of the calorimeter. Fig. 68 presents the dependence of  
 884 obtained energy resolution on the beam energy. The results of two fits are show. Left - the fit by the  
 885 function with the stochastic term only. Right - the fit by three-term function, including constant and noise  
 886 ones. One can see, that in both cases the stochastic term is about 56% which is very good agreement  
 887 with the simulation. The constant term of about 2.8% is obtained. This is rather small number. But it  
 888 shows, that the calorimeter is not totally compensated. Note, that the effect of constant term is significant  
 889 at high energies, where the stochastic term is negligible. For accurate estimation of the constant term  
 890 the measurements at high energies are desired. Also, as shown in Fig. 68, the noise term in energy  
 891 resolution is close to zero, that confirms the high light yield of the FHCAL modules and quality of the



**Fig. 65:** Energy spectra for 3 GeV/c proton in 9 cases – energy deposition in first section, sum of energy depositions in two first sections etc. up to sum of energy depositions in 9 sections.

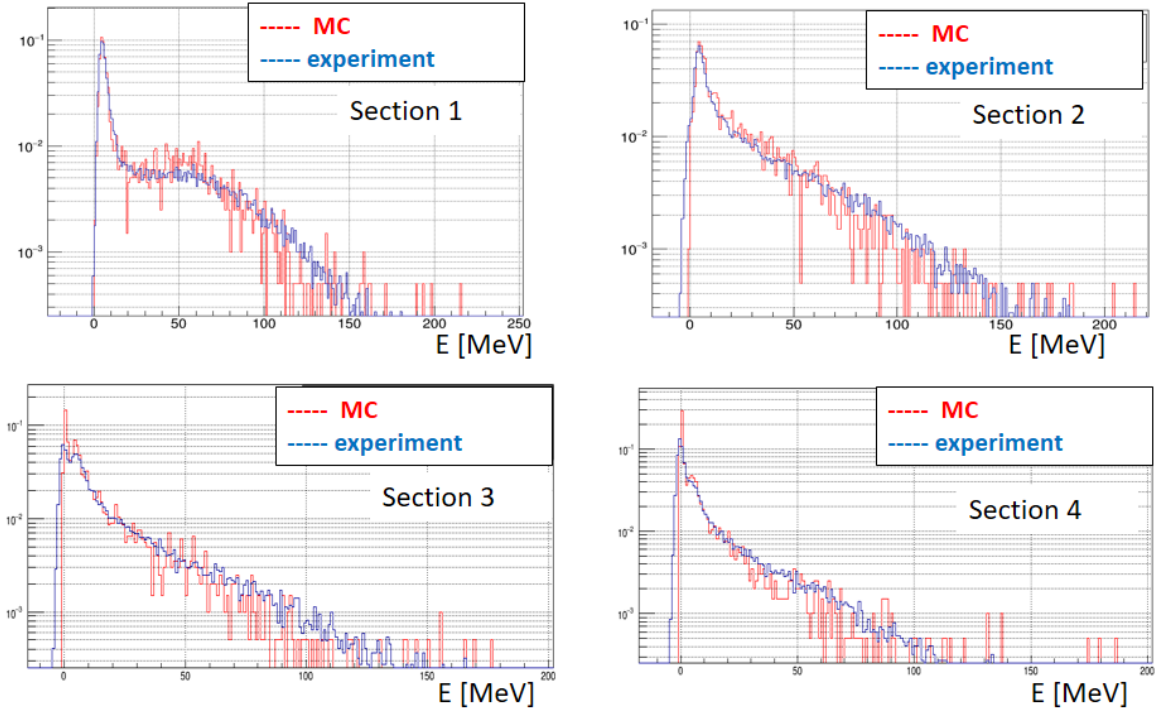


**Fig. 66:** Energy spectra for 6 GeV/c proton in 9 cases – energy deposition in first section, sum of energy depositions in two first sections etc. up to sum of energy depositions in 9 sections.

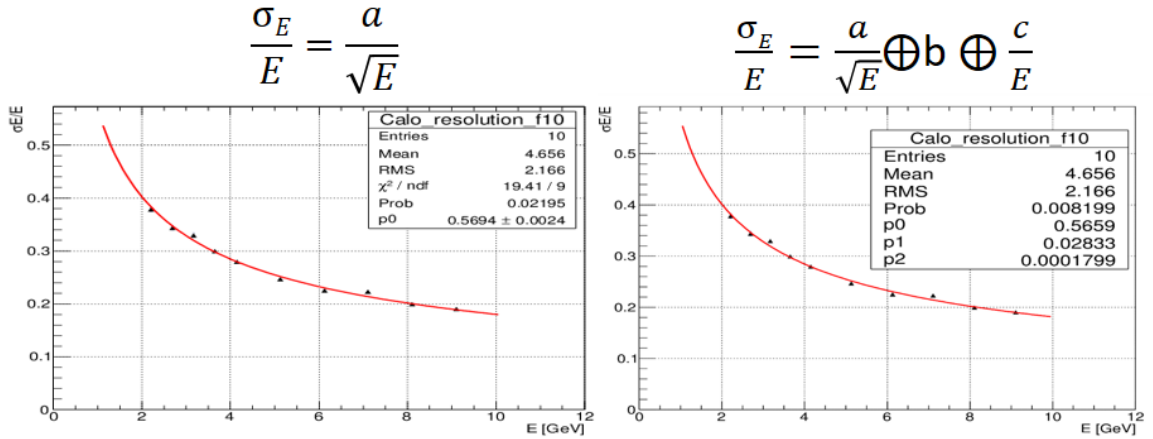
892 Front-End-Electronics.

893 The linearity of the calorimeter response to the hadrons with different energies is shown in Fig. 69 (left).  
 894 Here the dependence of mean value of the deposited energies on the beam energy is presented. As seen,  
 895 all the points are located near the straight line. Small deviations are observed for the lowest energies  
 896 where the contamination of the pions in proton data is possible due to the inefficiency of Cherenkov gas  
 897 counter in proton/pion identification.

898 The most interesting question is the minimum number of the longitudinal sections in modules to keep  
 899 the best FHCAL performance. The available space in magnet poles of the MPD magnet and interference

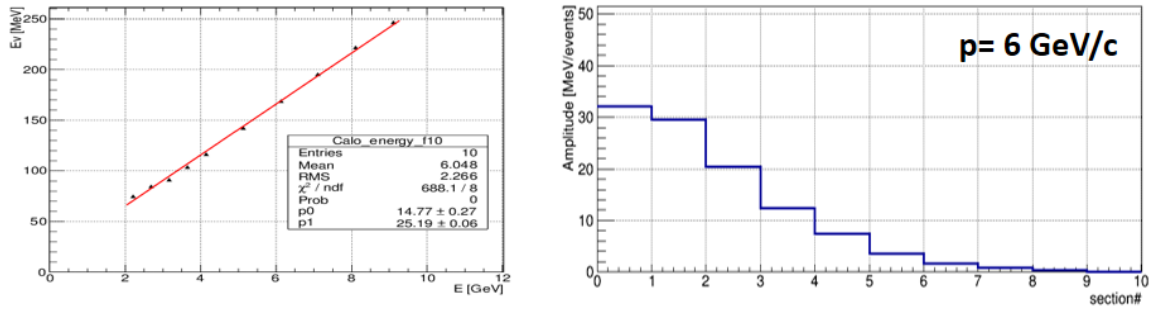


**Fig. 67:** Simulated and experimental energy spectra for 6 GeV/c proton in first four section.



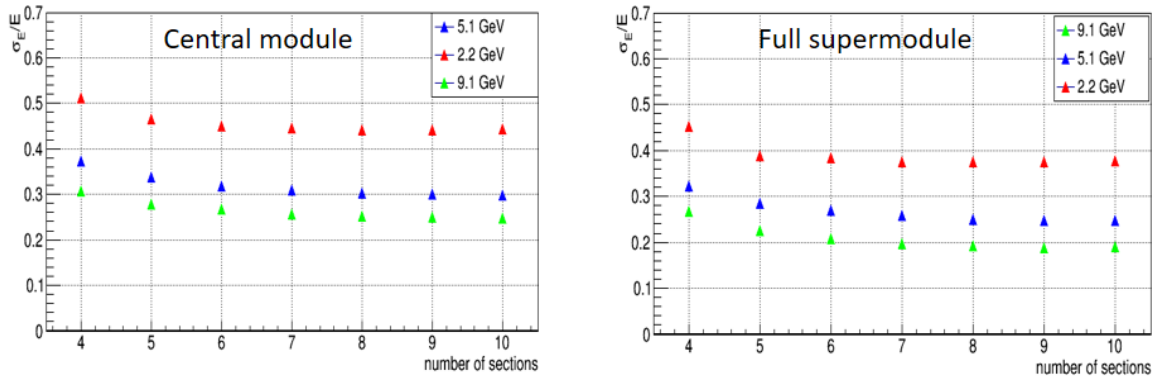
**Fig. 68:** Dependence of FHCAL energy resolution on the beam energy. The results of two fits are show. Left - fit by the function with the stochastic term only. Right- fit by three-term function, including constant and noise terms.

900 with beam elements behind the poles allow the installation of the FHCAL modules with 110 cm length  
 901 at maximum. The modules with 7 longitudinal sections can fit this restricted space. Fig. 70 presents  
 902 the dependence of the FHCAL resolution on the number of sections used in the analysis. One can see,  
 903 that withing the NICA beam energy range the energy resolution is practically unchanged for the last 4  
 904 sections. This is a natural sequence of the longitudinal shower profile for protons with low energies. Fig.  
 905 69 (right) shows such profile in central module for 6 GeV/c protons. As seen, the energy depositions in  
 906 the last 3 sections are negligible and their contribution to energy resolution must be minimum. These  
 907 observations confirm, that rather short modules with the 4 interaction lengths do not degrade the FHCAL



**Fig. 69:** Left - the dependence of mean value of the deposited energies on the beam energy. Right - the longitudinal hadron shower profile in central module for 6 GeV/c protons.

908 performance.



**Fig. 70:** Left - the dependence of mean value of the deposited energies on the beam energy. Right - the longitudinal hadron shower profile in central module for 6 GeV/c protons.

909 The FHCaL purpose is the measurement of a group of particles (projectiles) with the same energy. In this  
 910 case the final energy resolution for  $N$  particles will be defined as the energy resolution of single particle  
 911 divided by the square root of the number of particles:

$$\left| \frac{\sigma_E}{E} \right|_{N_{\text{particles}}} = \frac{1}{\sqrt{N}} \left| \frac{\sigma_E}{E} \right|_{1_{\text{particle}}} . \quad (14)$$

912 Obviously, the influence of the constant term is negligible in case of detection of a few particles. Note,  
 913 that the existence of a constant term in energy resolution is a general problem for most calorimeters. The  
 914 best lead/scintillator calorimeter prototype developed for JLC project, [9] has a constant term of 1 – 2%.  
 915 The lead/scintillating-fiber calorimeter [37] has a constant term of 2.5% and 1% before and after light  
 916 attenuation correction, respectively. A similar calorimeter of RD1 collaboration has a constant term of  
 917 1.8%.

## 918 6.5 Response of FHCaL module to photons

919 As mentioned above, the first section of FHCaL practically fully contains the energy of detected photons  
 920 and electrons and might be regarded as a electromagnetic calorimeter with crude sampling. The experi-  
 921 mentally measured energy resolution for the positrons is about  $\frac{\sigma_E}{E} = \frac{35\%}{\sqrt{E(\text{GeV})}}$ . In principle, one can try

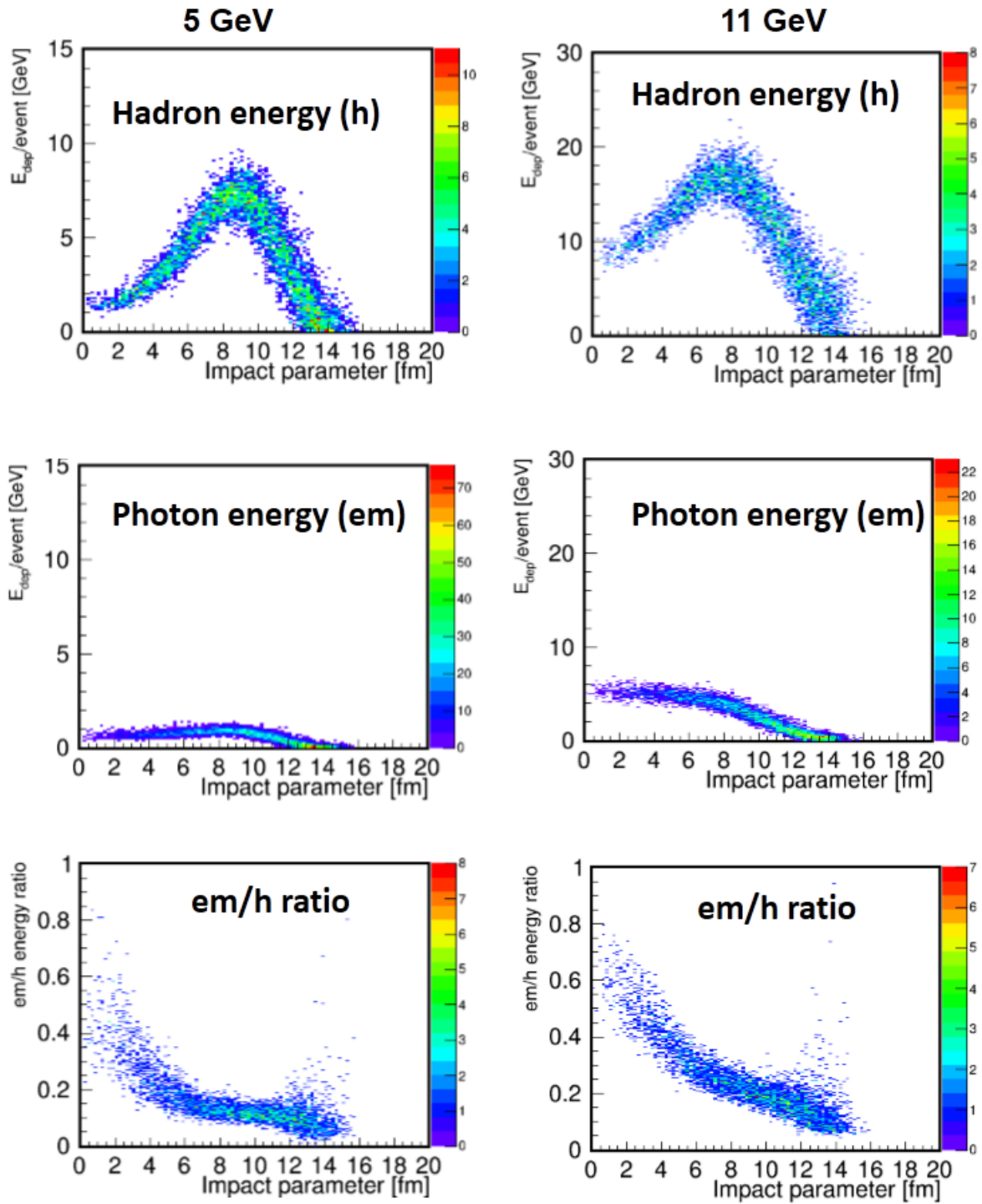


922 to make more sampling to detect the electromagnetic particles with better resolution. For example, in  
923 [9] the calorimeter prototype with 2 times finer sampling (8 mm lead and 2 mm scintillator) has energy  
924 resolution for a factor 1.5 better of about 24%.

925 In principle, the design of FHCAL modules allows the construction of more segmented first section with  
926 the 6 mm thick 12 layers of the absorber and with the full thickness  $12X_0$ . To check the performance  
927 of such ECAL, the response to e.-m. and hadron components was studied in the simulation. Fig.71  
928 presents the energy depositions in ECAL for e.-m. and hadron components separately and ratios of these  
929 components on event-by-event basis. Left and right panels correspond to beam energy  $\sqrt{s_{NN}} = 5$  GeV  
930 and  $\sqrt{s_{NN}} = 11$  GeV, respectively. One can see that e.-m. component alone can be used for the selection  
931 of the centrality because of the monotonic dependence on the impact parameter. Unfortunately, this  
932 component is small (about 20% for most part of events) fraction of the full energy deposited in first  
933 section. This is visible from the ratio of two components. As a result, the dependence of the full energy  
934 deposition on the impact parameter practically repeats the behavior of the hadron component.

935 These effects do not allow the use of the first section for the centrality selection. According to these re-  
936 sults, the fine segmentation of first section does not help in the improvement of the FHCAL performance.  
937 Moreover, construction of finely segmented first section would potentially spoil the performance of the  
938 hadron calorimeter itself because of about 20-30% of the hadron showers would deposit energy in the  
939 non-compensated part.

940 In conclusion of this chapter one can summarize, that the experimentally measured energy resolution of  
941 FHCAL prototype modules are about 60% for both low and high hadron energies. This resolution has no  
942 impact on the precision of the centrality determination. As shown in the beginning of the chapter, the  
943 spread of the detected energy in the calorimeter is determined by the fluctuations of the number of the  
944 spectators at some fixed value of impact parameter. This is a physical limitation in the accuracy of the  
945 centrality measurement. Further beam tests are planned with the FHCAL prototypes to exam the FEE and  
946 electronic readout performance at low energies. The especial importance is the electronic noise which is  
947 the main factor in the energy resolution at these energies.



**Fig. 71:** Dependence of energy depositions in first finely segmented sections on the impact parameter for hadrons and e.-m. particles. Also, the ratios of the electromagnetic and hadron energies on event-by-event basis are shown. Left and right panels correspond to beam energy  $\sqrt{s_{NN}} = 5$  GeV and  $\sqrt{s_{NN}} = 11$  GeV, respectively.

## 948 7 Subsystems of FHCAL

### 949 7.1 Control system

950 The gain of the FHCAL photodetectors (SiPMs or MAPDs) is very sensitive to both the applied bias  
 951 voltage and the environmental temperature. Therefore, a serious attention must be paid to the stability  
 952 of MAPD gains. For this purpose a FHCAL control and cooling system was developed. The gain  
 953 monitoring system includes a controlled power supply for MAPDs and the generator of stabilized light  
 954 pulses. For each MAPD the voltage is provided by a individual photodiode power unit mounted on the  
 955 printed circuit board near the photodetectors and managed by a separately placed common controller.  
 956 The power supply provides voltage in the range 60 – 80 V with accuracy about 10 mV. The maximum  
 957 current through each MAPD is 30 mA.

958 For the continuous monitoring of the photodiode gains a LED generator of stabilized light pulses has  
 959 been designed. It includes a pulse generator, a LED driver, a built-in PIN-photodiode, a QDC and a  
 960 microcontroller (see Fig. 72). The main part of the LED light is transferred through the optical clear  
 961 fibers to the individual MAPDs in the module, while a small part of the LED light is detected by a  
 962 PIN-photodiode and digitized by a QDC. To ensure the stability of the light pulse the QDC value is  
 963 permanently compared with the reference number. In case of a deviation between the QDC and the  
 964 reference values the microcontroller changes the LED driver amplitude in a proper way. The available  
 965 stabilized light pulser allows the long-term monitoring of the MAPD amplitudes, and, consequently, the  
 966 MAPD gain variations.

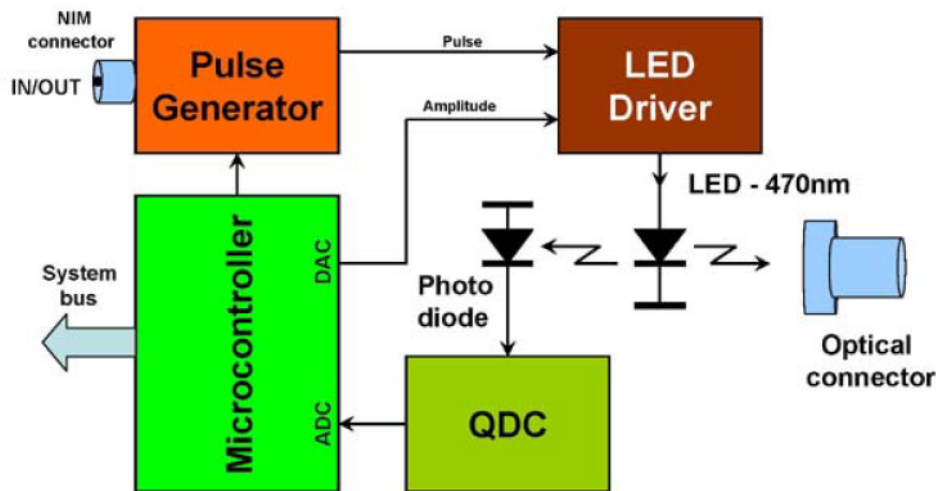


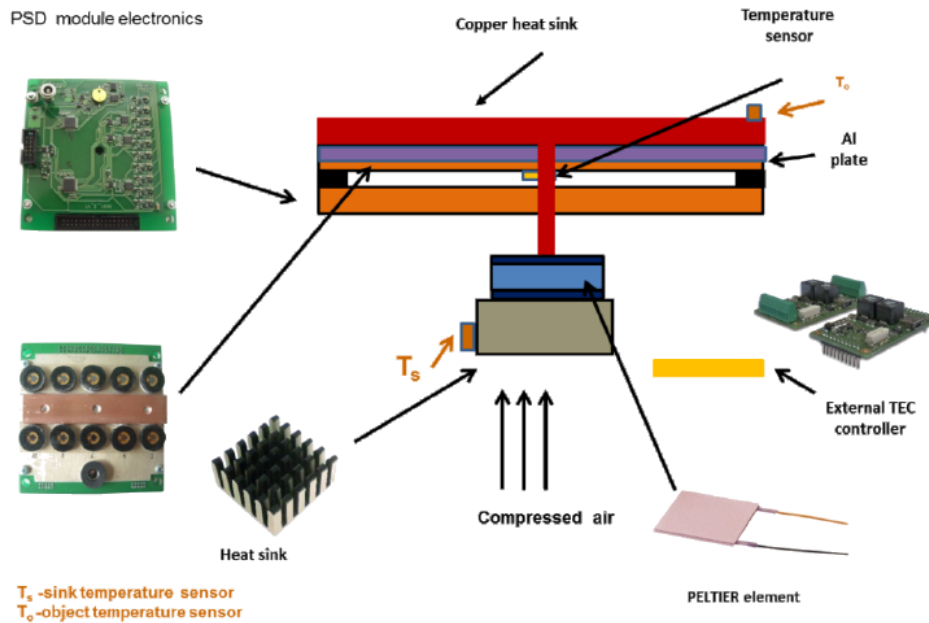
Fig. 72: Schematic diagram of the stabilized light source.

### 967 7.2 The photodetector temperature control system

968 Special attention should be paid to the SiPM (MAPDs) temperature stabilization, because these photodi-  
 969 odes have a gain temperature coefficient of about one percent per degree. Obviously, the temperature of  
 970 the photodiodes in each module must be stabilized and controlled with an accuracy of better than 1°.

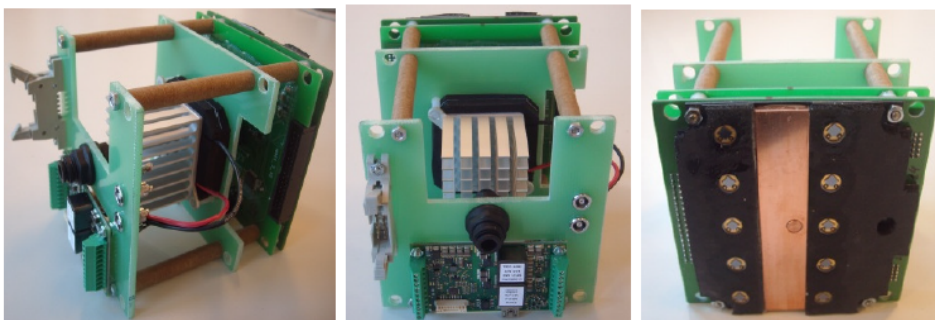
971 To fulfill this requirement a cooling system based on Peltier elements has been developed. The cooling  
 972 scheme is shown in Fig. 73. The photodiodes of one module are mounted on an aluminum plate that  
 973 provides a common thermal contact for all photodiodes in the module. This plate is cooled by a Peltier  
 974 element with a size of 30 × 30 mm<sup>2</sup>. One side of the Peltier element is glued by heat conducting adhesive  
 975 to a small copper plate which is connected by short copper rods (diameter 6 mm) to other large copper

976 plate glued to the aluminum plate. This copper rod passes through hole in the center of the electronic  
 977 board. The large copper plate is placed in the gap between the two rows of photodiodes mounted on the  
 978 aluminum plate. All open surfaces of aluminum and copper plates, as well as the copper rod are carefully  
 979 thermally insulated by armaflex. The temperature of the aluminum plate with the attached photodiodes  
 980 is measured by the temperature sensor, placed on the same plate. Another temperature sensor is mounted  
 981 on the heat sink, which is glued to the other (hot) side of the Peltier element. For a more efficient cooling  
 982 compressed air is blown onto the sink. The current through the Peltier element and the temperature  
 983 values provided by 2 t-sensors are read out by a TEC-controller [38].



**Fig. 73:** Schematic view of the assembled electronics and cooling system based on the Peltier element. Explanations are given in the text.

984 A photo of the assembled electronics with cooling and temperature stabilization system is shown in Fig.  
 985 74 (left). The panel with the installed TEC controller is shown in Fig. 74 (middle). The location of 10  
 986 photodiodes mounted on an aluminum plate is shown in Fig. 74 (right).



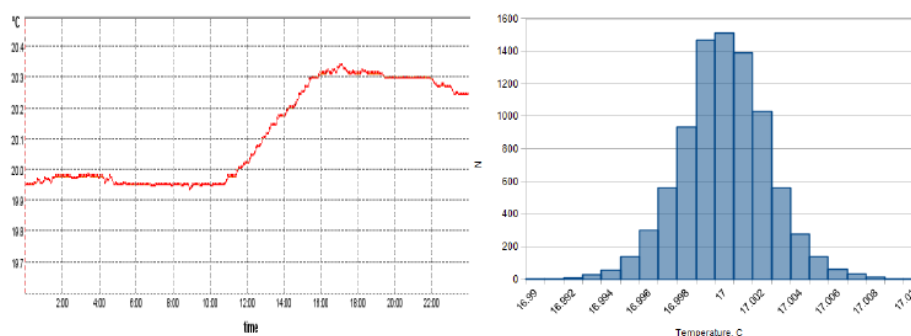
**Fig. 74:** Left picture: photo of the assembled prototype electronics, cooling and temperature stabilization system for one calorimeter module. Center picture: photo of TEC controller on the panel. Right picture: view of the front aluminum plate with 10 MAPDs. The copper plate is visible in the middle of two MAPDs rows.

987 The copper plate is adhered to an aluminum plate between two rows of photodiodes. All the exposed

988 parts are isolated by armaxflex.

989 The control electronics with the cooling system is placed in the calorimeter module to provide the op-  
 990 tical contact of MAPDs mounted on the aluminum plate to the respective optical connectors. The Fig.  
 991 75 demonstrates some results of test measurements of long-term stability of the cooling system. The left  
 992 panel of Fig. 75 shows the change of room temperature as a function of time (during 24 hours of con-  
 993 tinuous measurements). The room temperature varies during the measurement between  $19.5^\circ$  and  $20.5^\circ$ .  
 994 The temperature of the aluminum plate with the photodiodes was set to  $17^\circ\text{C}$  by the TEC controller.

995 The variation of the temperature recorded during 24 hours by the t-sensor on the aluminum plate is shown  
 996 in the right panel of Fig. 75. It is seen that the average temperature is  $17^\circ$ , and the width is less than  $0.1^\circ$ .  
 997 The data demonstrate that the cooling system provides the requested long-term temperature stabilization  
 998 of photodiodes.

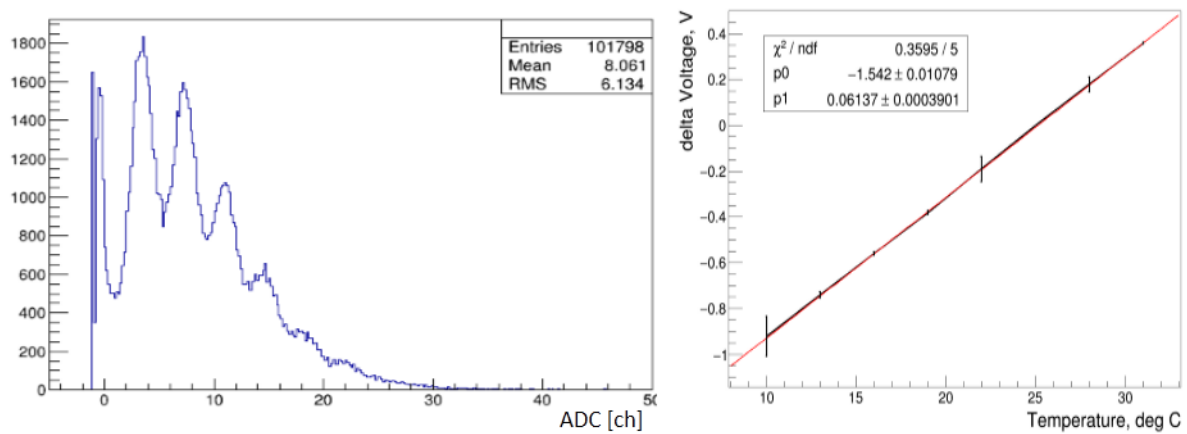


**Fig. 75:** Left panel: the room temperature as a function of time (during 24 hours of continuous measurements). Right panel: the temperature variation measured by the t-sensor on the aluminum plate.

999 There is another direct method of the SiPM gain stabilization at the non-stable environmental temperature  
 1000 which is already applied in a few setup last years. This method is based on a simple correction of  
 1001 the applied voltage. According to the theoretical models and the experimentally measured results, the  
 1002 breakdown voltage of SiPM is proportional to the temperature. The proportional dependence is preserved  
 1003 for any SiPM/MAPD type. In our case, the dependence of the corrected voltage on the temperature was  
 1004 measured for Hamamatsu MPPC S12572-010C/P and is presented in Fig. 76.

1005 For this goal, the gain of MPPC was measured with the help of ADC spectrum from a low intensity LED  
 1006 pulse (Fig. 76, left). Depending on the MPPC temperature and gain the distance between the peaks in  
 1007 ADC spectrum is changing. To stabilize the MPPC gain a corrected voltage is applied. The dependence  
 1008 of the corrected voltage on the surrounding temperature is shown in Fig. 76, right. One can see, that the  
 1009 voltage gradient is about  $60\text{ mV}/^\circ\text{C}$ .

1010 At present, we developed a slow control system that readouts the SiPM temperature and corrects the  
 1011 applied voltage. The reliability of the developed method is currently tested.



**Fig. 76:** Left panel: the ADC spectrum from a detected by MPPC a few photon LED pulse. The peaks correspond to the different number of detected photons. The distance between the peaks depends on the MPPC gain. Right panel: the dependence of the corrected voltage on the MPPC temperature.

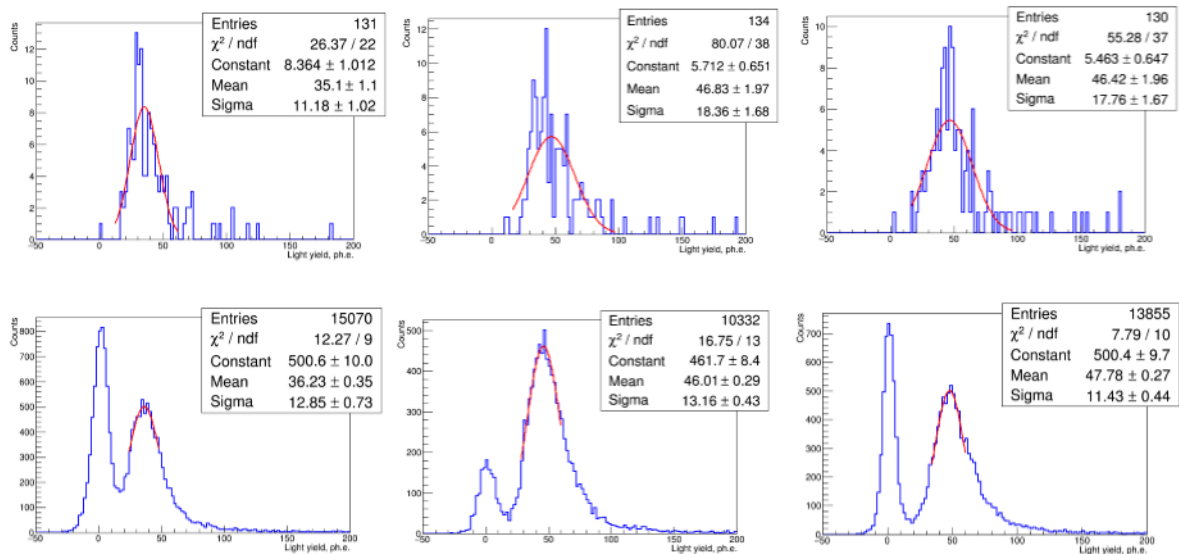
### 1012 7.3 Calibration method

1013 The energy calibration of FHCAL is a challenging task because the calorimeter is placed in the magnet at  
 1014 fixed position and cannot be moved in transverse direction to perform the beam scan of FHCAL module.  
 1015 Also, the beam pipe crosses the central module and doesn't allow the movement of the FHCAL. The  
 1016 only choice for the calibration is the use some process with known energy deposition in FHCAL module  
 1017 sections.

1018 As was discussed above, the tests of FHCAL module prototypes with cosmic muons reveal a nice op-  
 1019 portunity to use muons (or the minimum ionizing particles) for the energy calibration. Nice peaks in  
 1020 amplitude spectra from 5 MeV muon energy depositions in the longitudinal sections present an excel-  
 1021 lent tool for the absolute energy calibration. This possibility provides a nice opportunity to calibrate the  
 1022 FHCAL modules with the cosmic muons.

1023 The cosmic muons deposit different energy in scintillators depending on the track lengths inside the  
 1024 longitudinal section of the module. For this reason we selected two types of the muon tracks. First class  
 1025 of events are cosmic muons passed through all 7 longitudinal sections of the FHCAL module, see Fig. 77,  
 1026 top panels. Unfortunately the statistics for two days of the data collection is only about 130 events per  
 1027 section. Nevertheless, the amplitude peaks are nicely fitted providing the absolute light yield of about  
 1028 35-45 photoelectrons per 5 MeV of deposited energy. To speed up the calibration procedure another  
 1029 class of the events was considered. In this case the inclined muon tracks passed through the calibrated  
 1030 section and the neighbor two sections were selected, Fig. 77, down panels. The statistics there is two  
 1031 orders higher that allow the calibration for a one hour of the data taking. As seen, both methods provides  
 1032 the same light yield withing 1-2% of accuracy.

1033 The developed calibration procedure allows a permanent control of the calibration coefficients as well as  
 1034 the MPPC gain monitoring.

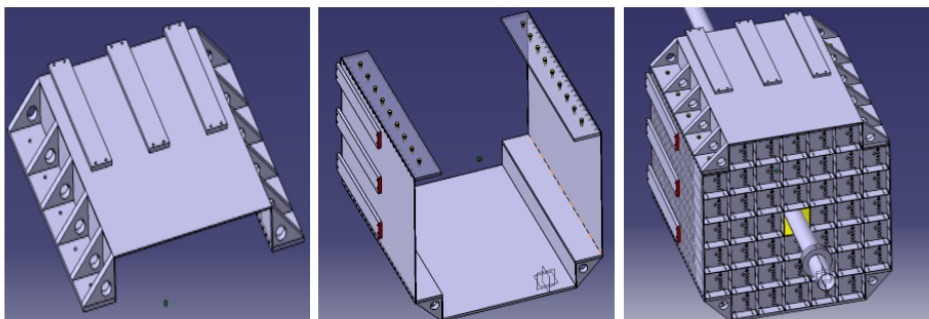


**Fig. 77:** A few ADC spectra from the cosmic muons passed through longitudinal sections of the FHCAL module. Top panels: for horizontal muons crossed all 7 sections of the module. Down panels: for the inclined muon tracks passed through the calibrated section and the neighbor two sections. Peaks near zero are ADC pedestals.

#### 1035 7.4 FHCAL mechanical support

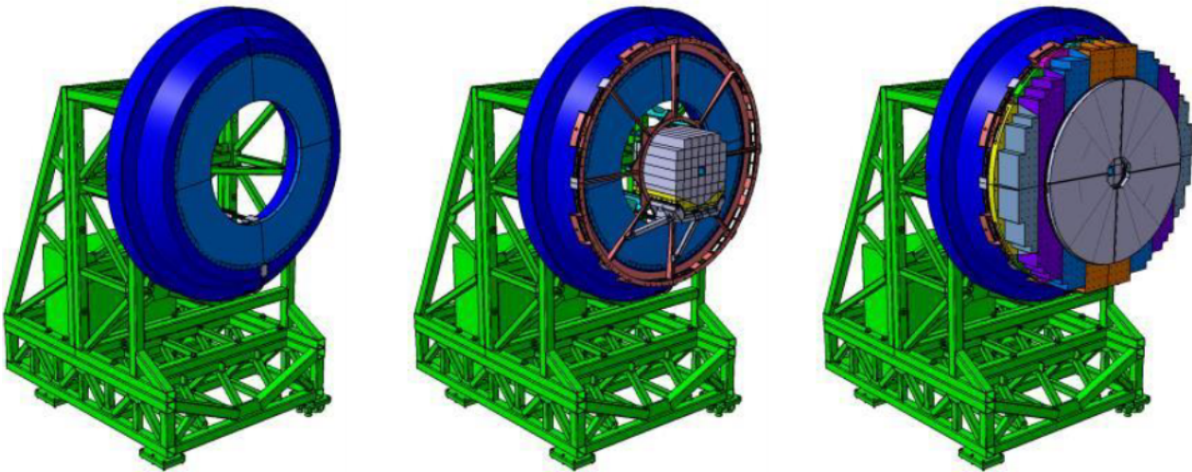
1036 FHCAL will consist of two left/right symmetrical parts. Two independent mechanical platforms are  
 1037 needed for the support of the calorimeter and its positioning respective the beam line. Each calorimeter  
 1038 part has a weight of about 8.5 tons and requests the corresponding support structure. The platform must  
 1039 have the ability to move in forward/backward direction to install/uninstall the FHCAL in the magnet.  
 1040 Also, the support platform must be able to adjust the FHCAL position in transverse X- and Y-directions  
 1041 with the precision of about 1 mm. Such feature is needed for the adjustment of the FHCAL beam hole  
 1042 with the beam pipe of the accelerator that crosses through the central modules of the calorimeter parts.

1043 For this goal a few mechanical elements were designed and a procedure of the FHCAL installation is  
 1044 developed. At first stage the FHCAL modules are installed inside the support, see Fig. 78.



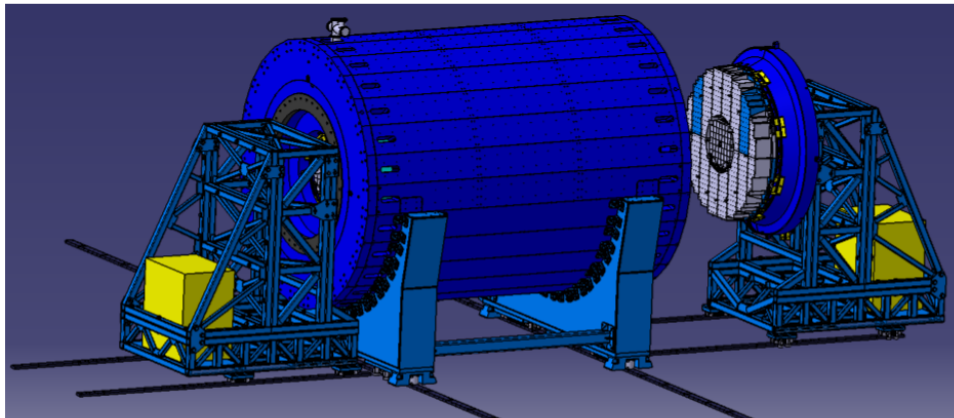
**Fig. 78:** Support for FHCAL modules.

1045 Then, the support with FHCAL modules is mounted into the magnet encup pole, where the ECAL and  
 1046 TOF endcap is installed also, Fig. 79.



**Fig. 79:** Magnet pole alone (left), with FHCAL (middle) and endcup detectors (right).

1047 Finally, magnet pole with the detectors is inserted into magnet, Fig. 80.



**Fig. 80:** Installation of the endcup pole into the magnet.

1048 Note, that this FHCAL installation scheme is not finally established and might be modified.

## 1049 7.5 FHCAL trigger

1050 The important task in MPD experiment is the detection of the events in a maximum range of the impact  
 1051 parameters, in particularly, of the peripheral collisions with  $b > 10 fm$ . In this case, the deposited in the  
 1052 MPD sub- detectors energies are essentially smaller comparing to that in central collisions. It makes the  
 1053 problem in the arrangement of the trigger for these peripheral events. For this reason the possibility to  
 1054 include FHCAL in the trigger was studied.

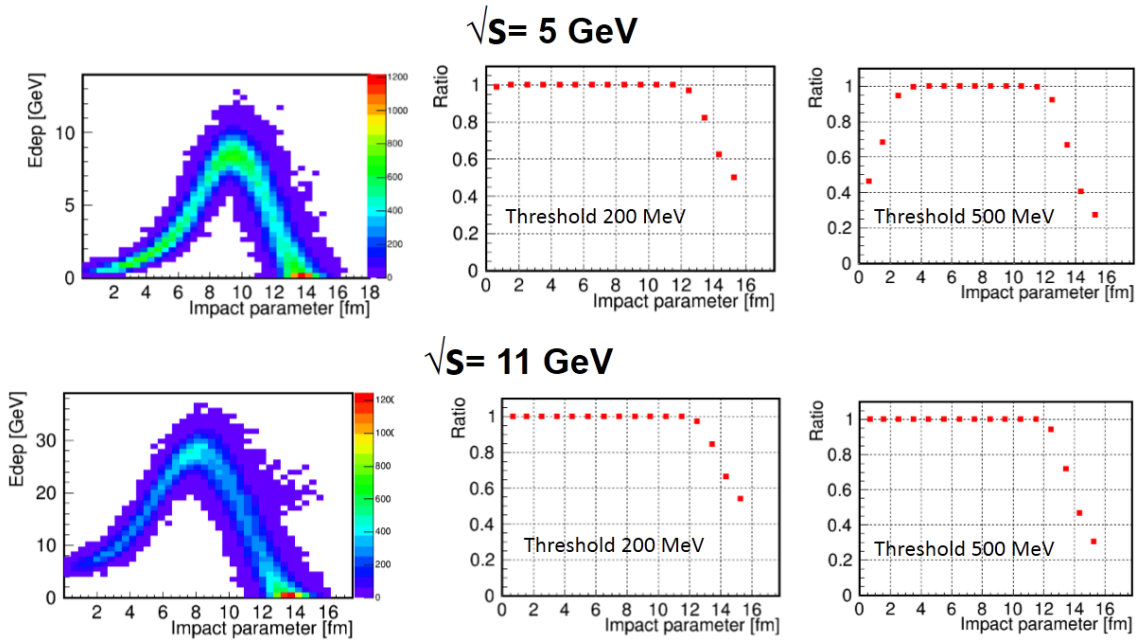
1055 In the peripheral collisions the spectator energy is mainly deposited around the beam hole in 8 central  
 1056 modules. Therefore, the dependence of the detected energy in these central modules on impact parameter  
 1057 was simulated, Fig. 81. As seen, the energy deposition in 8 central modules is above a few hundred MeV  
 1058 up to  $b = 12 fm$ . Note, that the deposited (or detected) energy is only about 2.5% from the initial hadron  
 1059 energy because the most part is absorbed in the lead plates as discussed in previous chapter.



1060 The FHCAL trigger threshold must be as low as possible to detect the most peripheral events. At the  
 1061 same time, this threshold must be higher of the possible electronic noises. One can make a conservative  
 1062 estimation of the electronic noise for 8 central modules. According to the tests of the FHCAL modules  
 1063 with the cosmic muons, the energy deposition of 5 MeV corresponds to the signal amplitude of about  
 1064 50 photoelectrons, i.e. 10 ph.e./MeV. The electronic noise in one channel (section) is below 10 photo-  
 1065 electrons or 1 MeV. 8 modules or 56 sections would have the uncorrelated noise below 10 MeV. For the  
 1066 safety reason and also to exclude the influence of the correlated noises, the threshold might be one order  
 1067 higher or above 100 MeV.

1068 To calculate the efficiency of FHCAL trigger at different thresholds on the energy deposition, the ratio of  
 1069 the events above threshold to the events without threshold was plotted, Fig. 81 middle and right panels.  
 1070 One can see, that up to  $b = 12\text{fm}$  the trigger efficiency is practically 100% for both 200 MeV and  
 1071 500 MeV thresholds on the detected energy. For the most peripheral events with the impact parameter  
 1072  $b > 12\text{fm}$  the trigger efficiency drops significantly. As follows from these data, the FHCAL trigger might  
 1073 be used for the trigger of the peripheral collisions with  $b < 12\text{fm}$ .

1074 Note, that the Front-End-Electronics has an analog sum of the signals from 7 longitudinal sections.  
 1075 Therefore, at the hardware level one can easy arrange the energy threshold for any number of the FHCAL  
 1076 modules.



**Fig. 81:** Left plots: Dependence of the detected energies in 8 closest to the beam modules on the impact parameter. Middle plots: ratios of the number of events with/without 200 MeV threshold on the deposited energies in 8 closest to the beam modules. Right plots: ratios of the number of events with/without 500 MeV threshold on the deposited energies in 8 closest to the beam modules. Top and down panels correspond to beam energy  $\sqrt{s_{NN}} = 5\text{ GeV}$  and  $\sqrt{s_{NN}} = 11\text{ GeV}$ , respectively.

1077 **8 Timetable and cost estimation**

1078 Time schedule and the cost estimation for the FHCAL construction, assembly and operation is presented  
 1079 in Fig. 82. According to the plans, the production of the FHCAL components (lead absorbers, scintillator  
 1080 tiles, etc.) starts in 2017. The assembling of all modules will be finished in 2019. Also the mechanical  
 1081 platform will be constructed that time. The full commissioning of the calorimeter is planned to start  
 1082 in 2020. The total cost of FHCAL production, assembling, construction of the mechanical platform,  
 1083 commissioning and operation during first few years is 1750 k\$.

	2017	2018	2019	2020	2021	2022	Cost k\$
lead absorbers							180
scintillator tiles							170
WLS-fibers							120
mechanical components							160
optical elements							90
Infrastructure for module assembling							150
assembling of modules							320
Analog electronics							160
Readout electronics							150
Construction of FHCAL platform							170
FHCAL commissioning							40
FHCAL operation							40
Cost k\$	700	450	475	45	40	40	1750

Fig. 82: Time schedule and cost estimation for the FHCAL construction, assembly and tests.

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